

TESCO METERING

THREE PHASE THEORY

TESCO's Meter School

TESCOOL

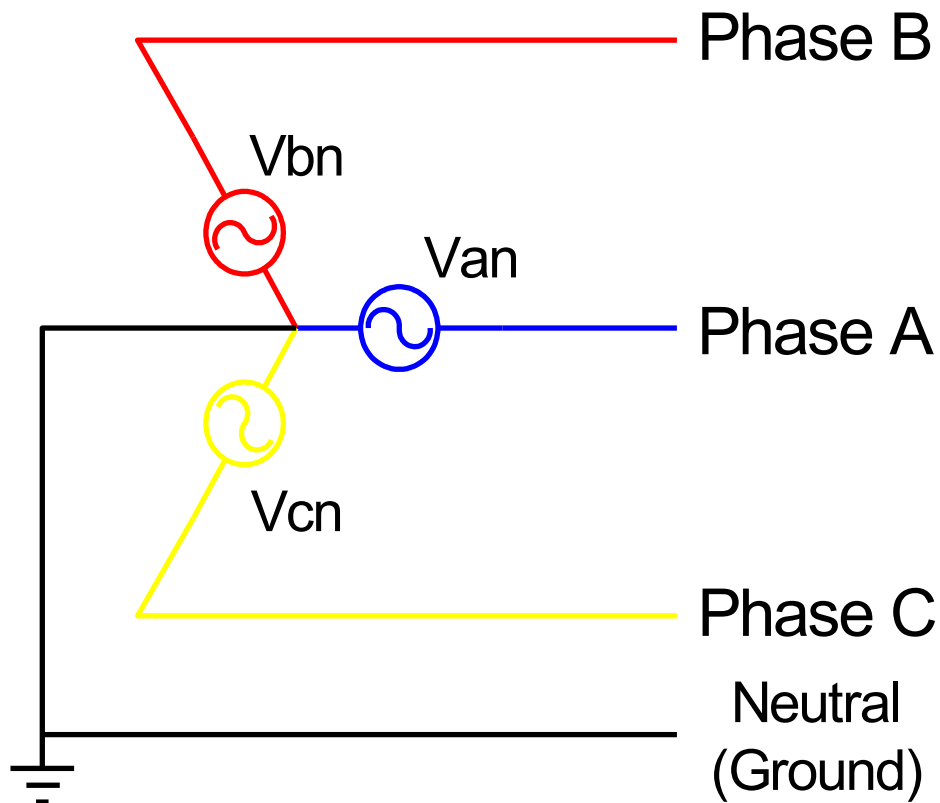
July 21-24, 2024

Monday, July 22, 2024

1:00 PM – 2:30 PM

Pete Brown

THREE PHASE POWER INTRODUCTION



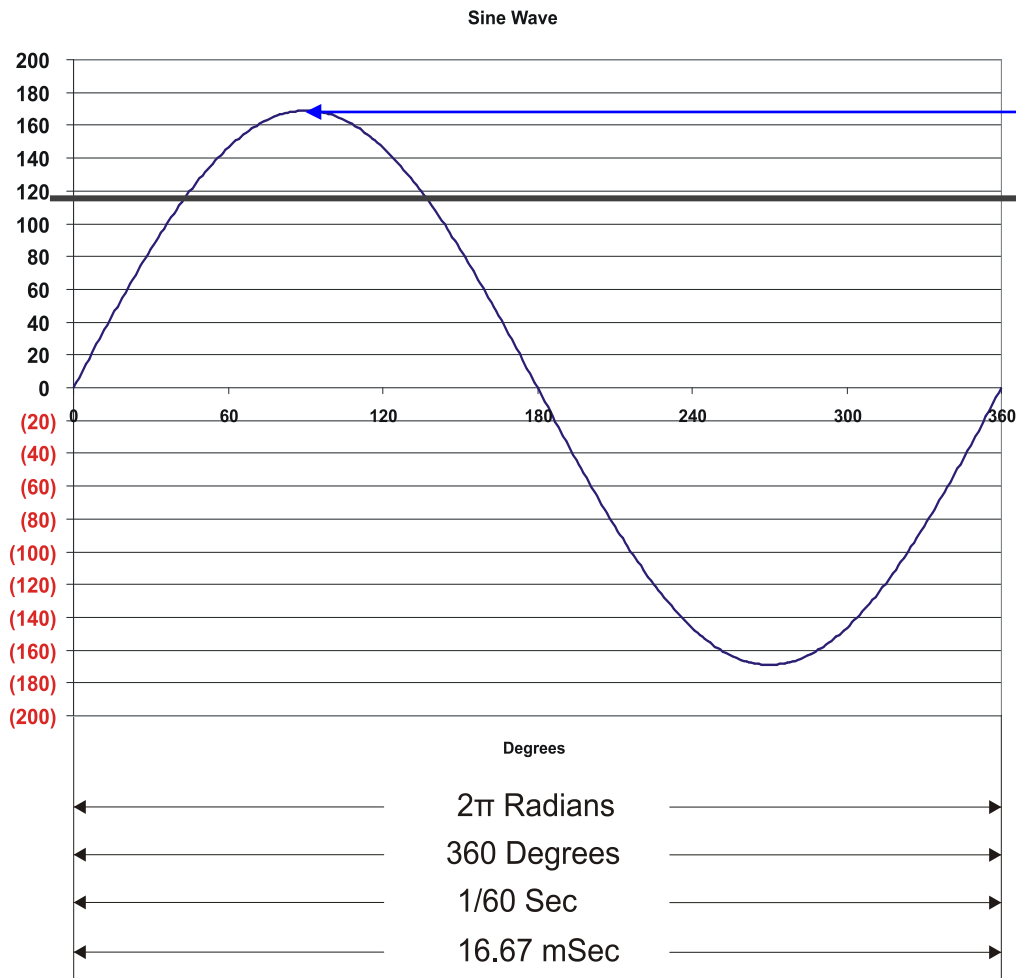
Basic Assumptions

- Three AC voltage sources
- Voltages Displaced in time
- Each sinusoidal
- Identical in Amplitude



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AC THEORY – SINE WAVE



$$V = V_{pk} \sin(2\pi ft - \theta)$$

$$V = \sqrt{2} V_{rms} \sin(2\pi ft - \theta)$$

$$V_{rms} = 120$$

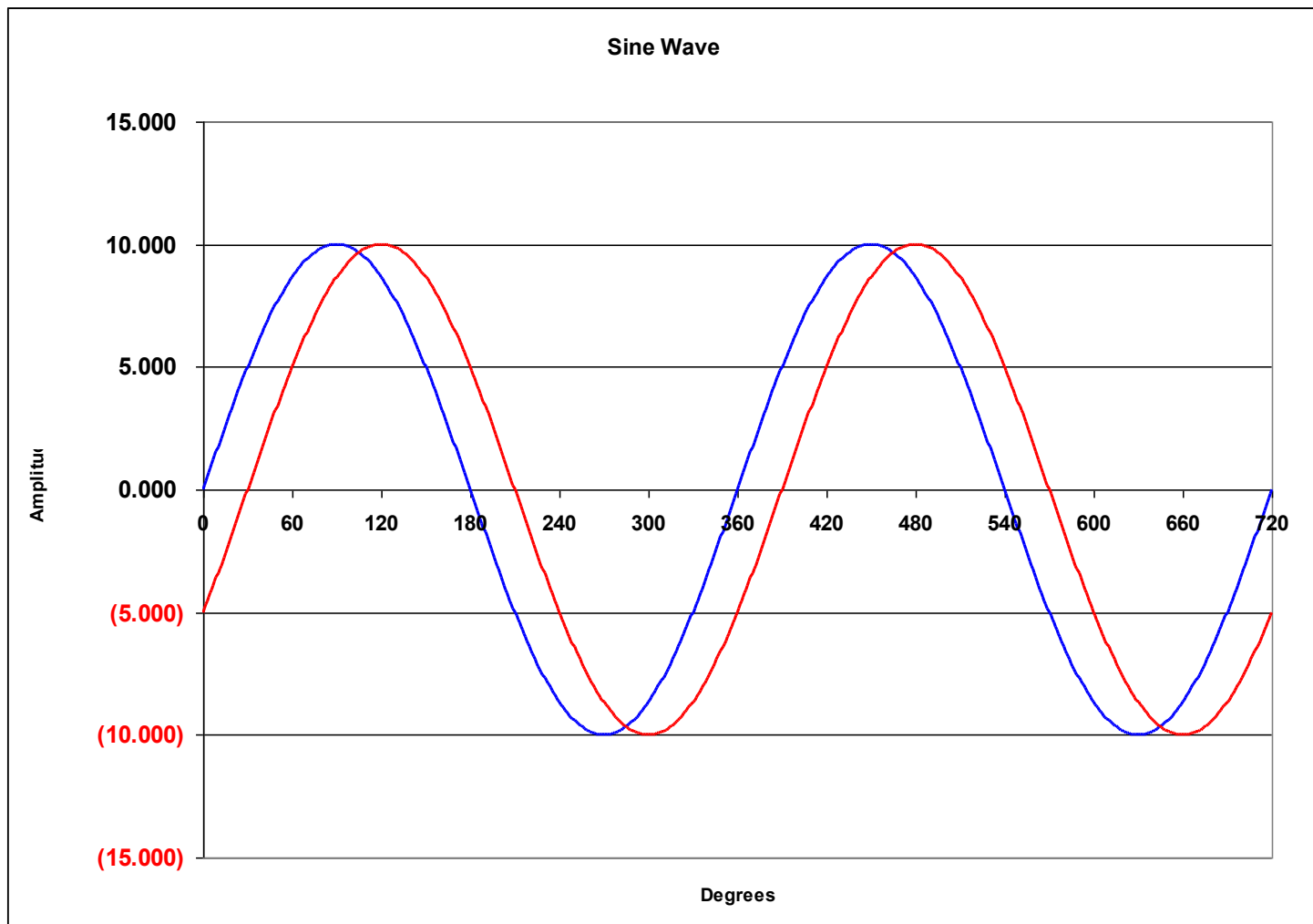
$$V_{pk} = 169$$

$$\theta = 0$$



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AC THEORY - PHASE

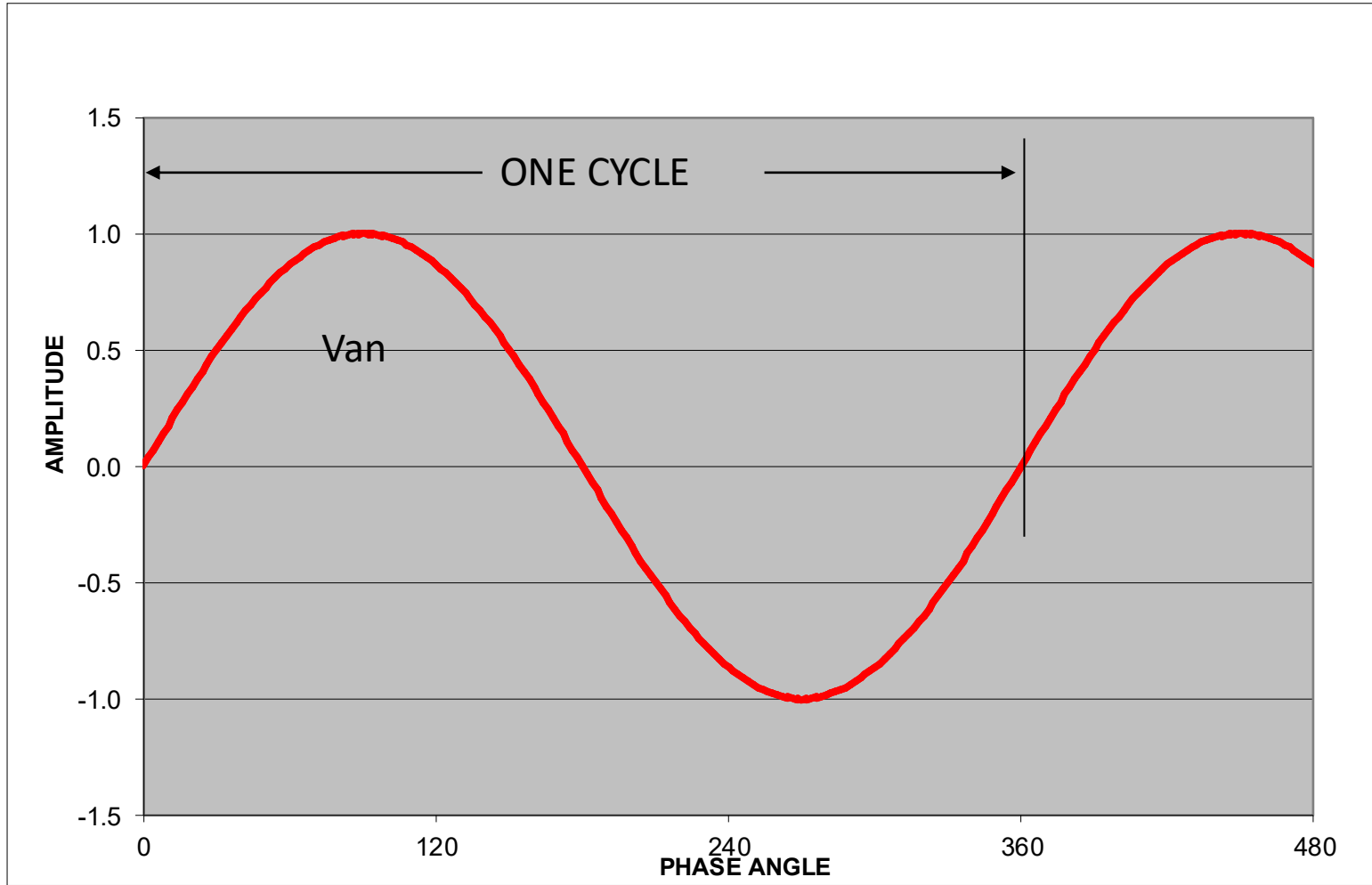


$$V = 10 \sin(2\pi ft)$$

$$V = 10 \sin(2\pi ft - 30)$$

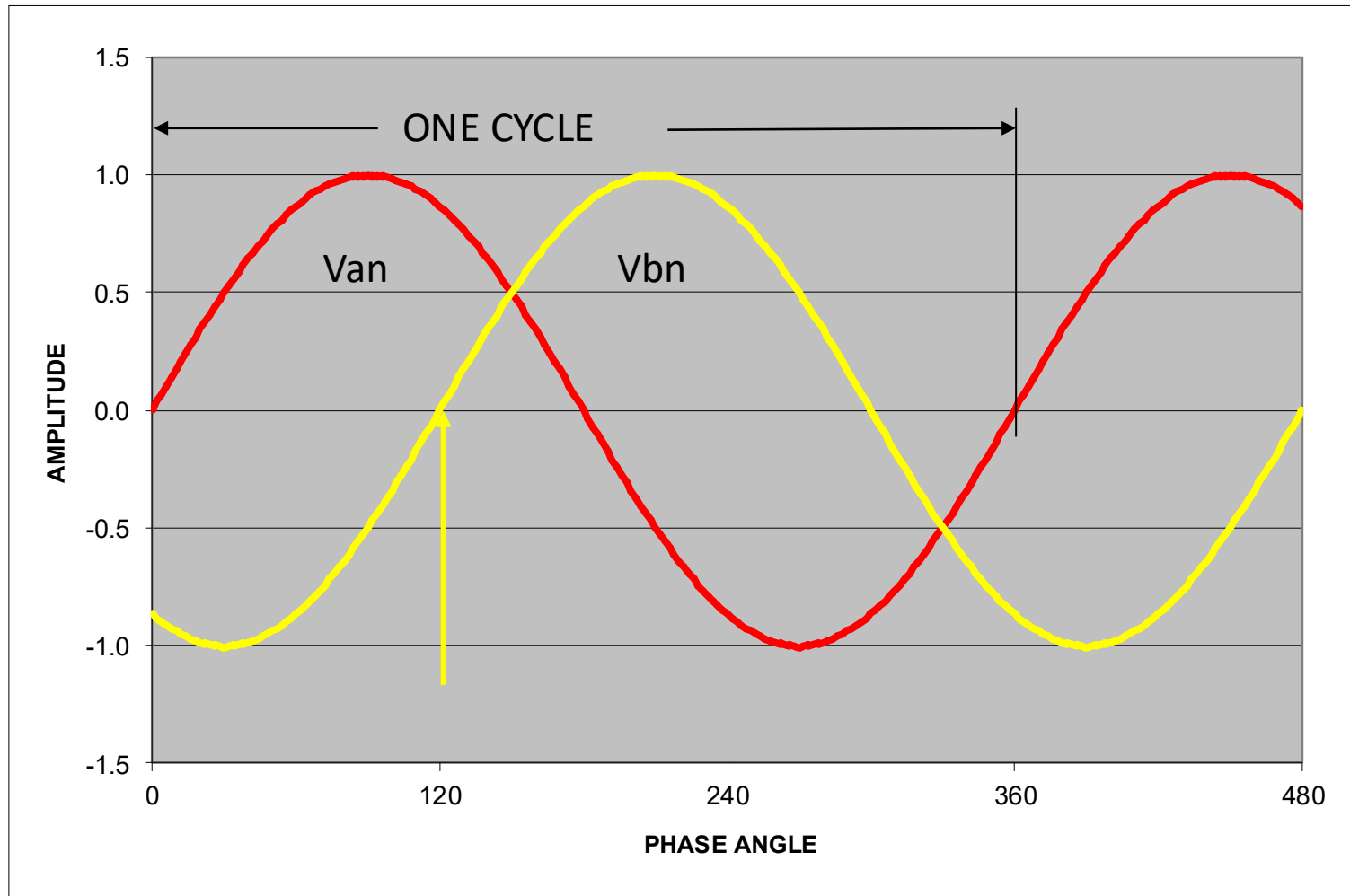
THREE PHASE THEORY

SINGLE PHASE - VOLTAGE PLOT



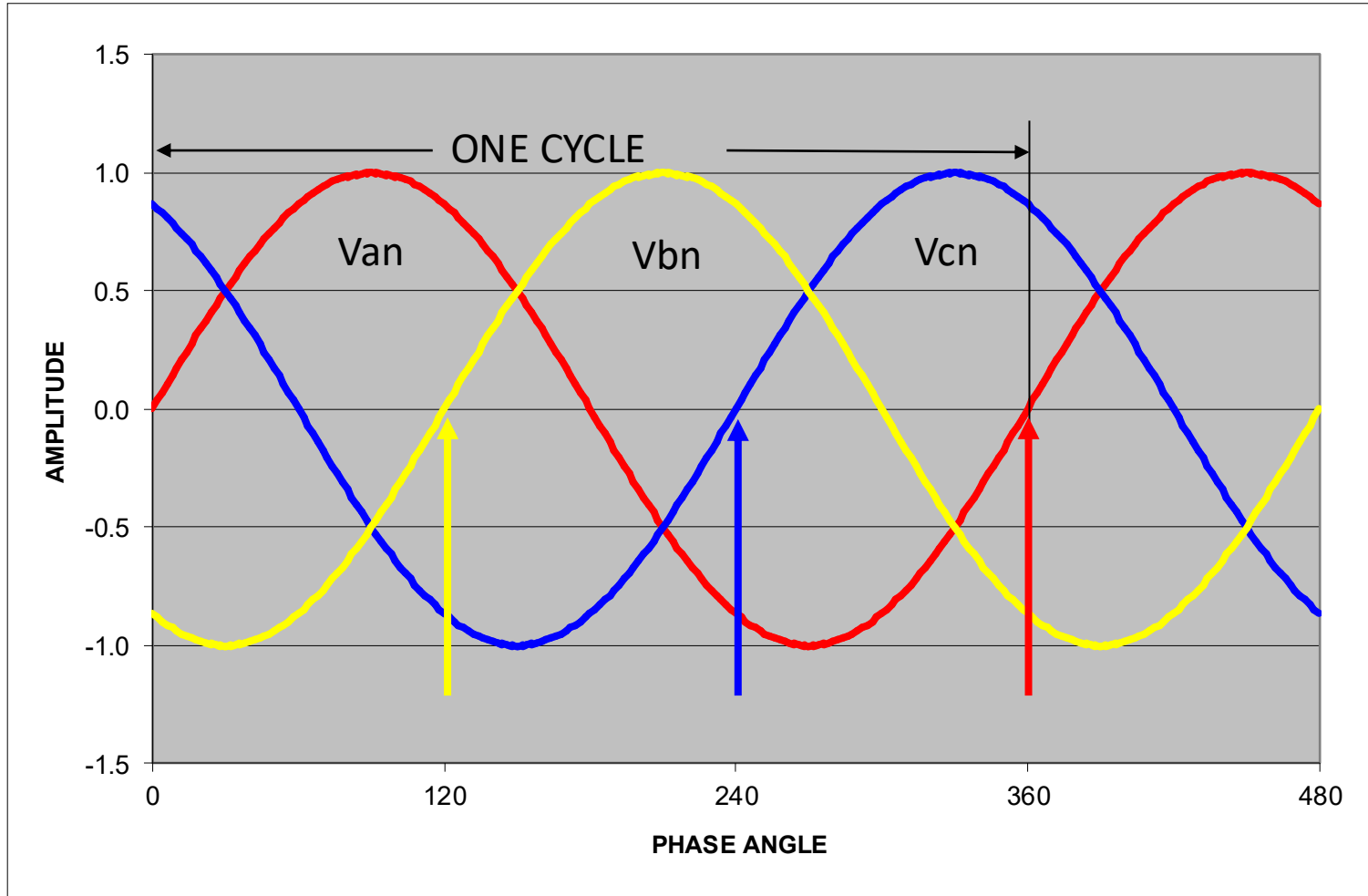
THREE PHASE THEORY

TWO PHASES - VOLTAGE PLOT



THREE PHASE THEORY

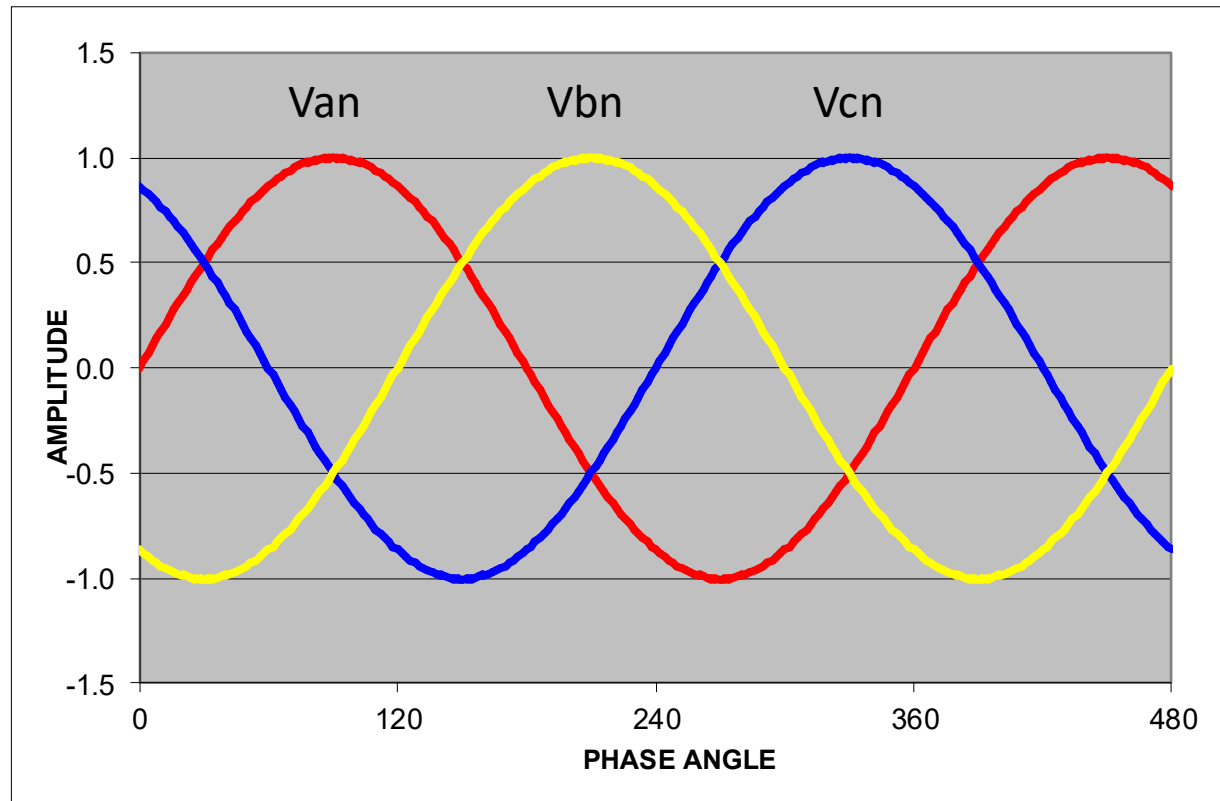
THREE PHASE - VOLTAGE PLOT



THREE PHASE POWER

AT THE GENERATOR

Three voltage vectors
each separated by 120° .
Peak voltages essentially
equal.



Most of what makes three phase systems seem complex is what we do to this simple picture in the delivery system and loads.

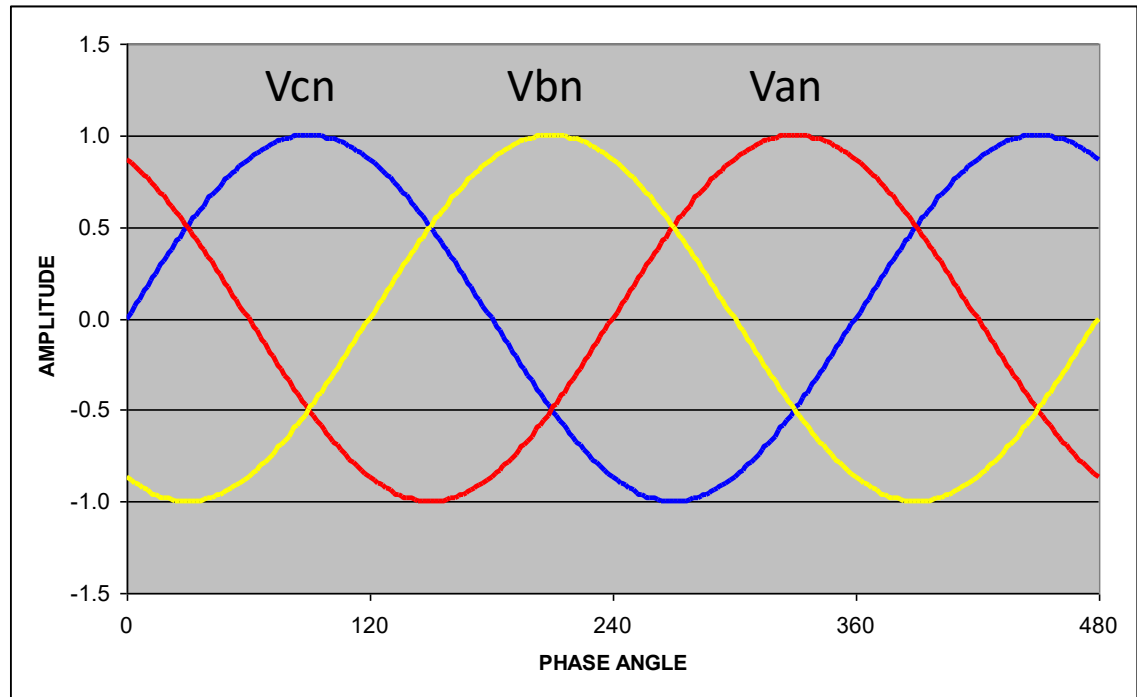
Phase Rotation:

The order in which the phases reach peak voltage.

There are only two possible sequences:

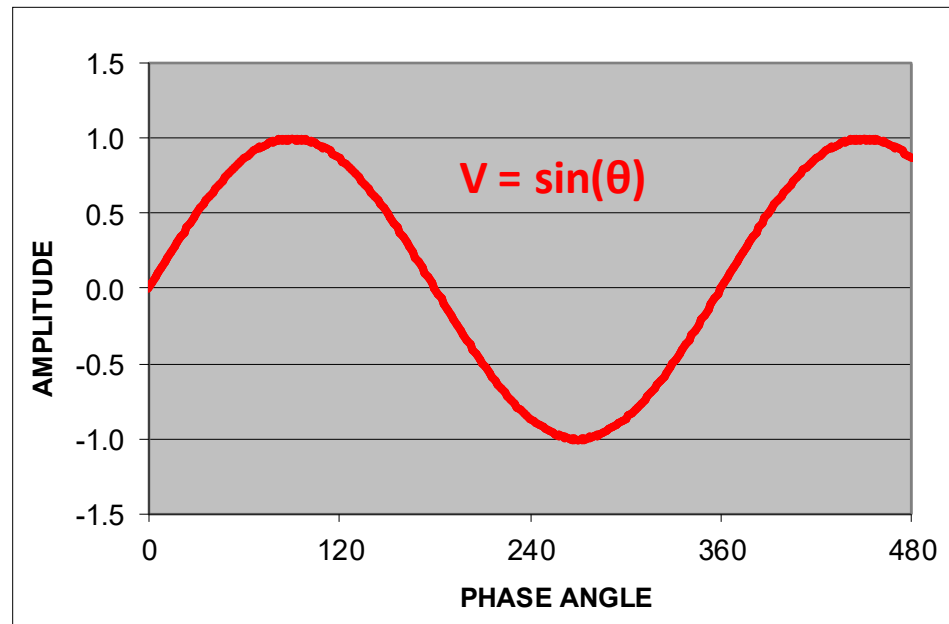
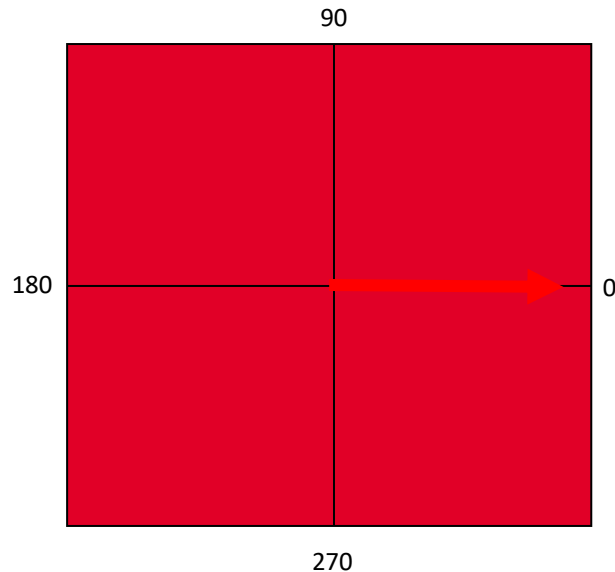
A-B-C (previous slide)

C-B-A (this slide)

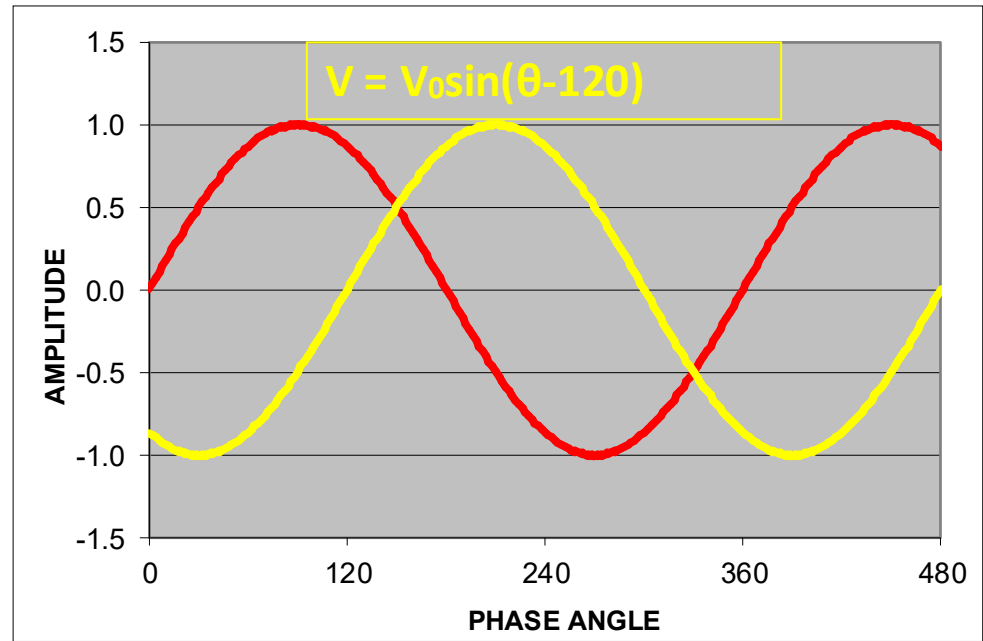
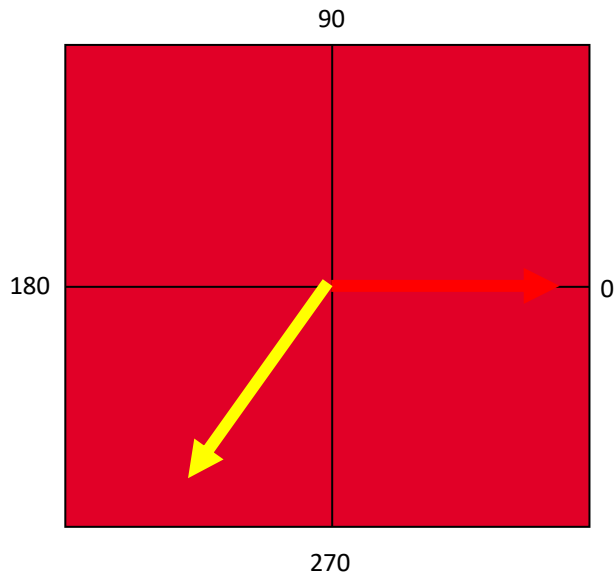


Phase rotation is important because the direction of rotation of a three phase motor is determined by the phase order.

- Phasors are a graphical means of representing the amplitude and phase relationships of voltages and currents.



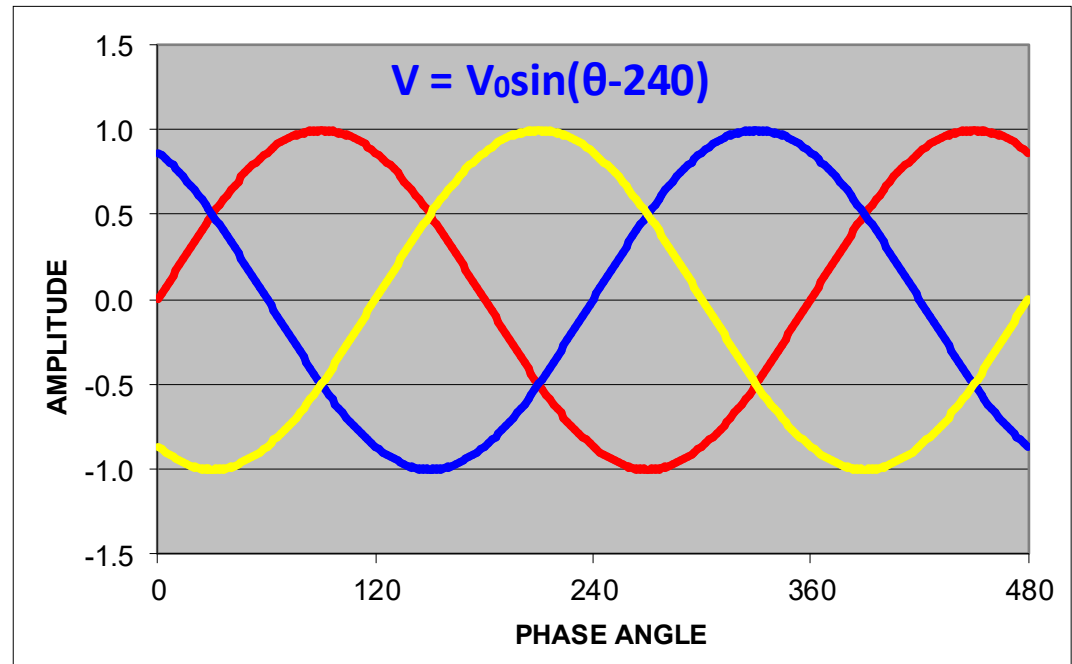
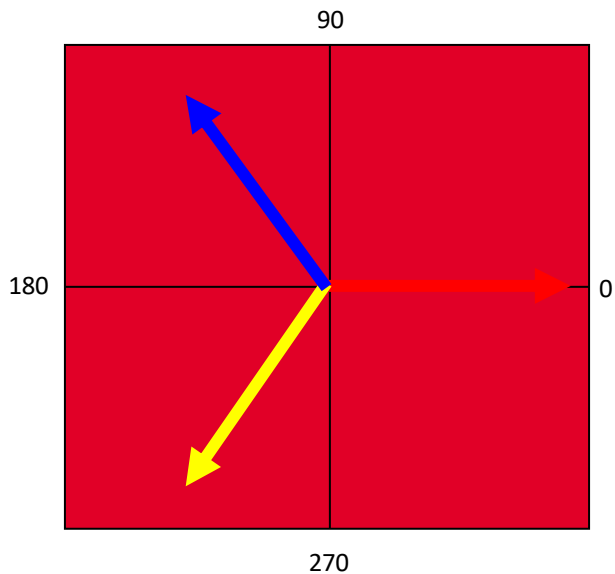
- As stated in the Handbook of Electricity Metering, by common consent, counterclockwise phase rotation has been chosen for general use in phasor diagrams.



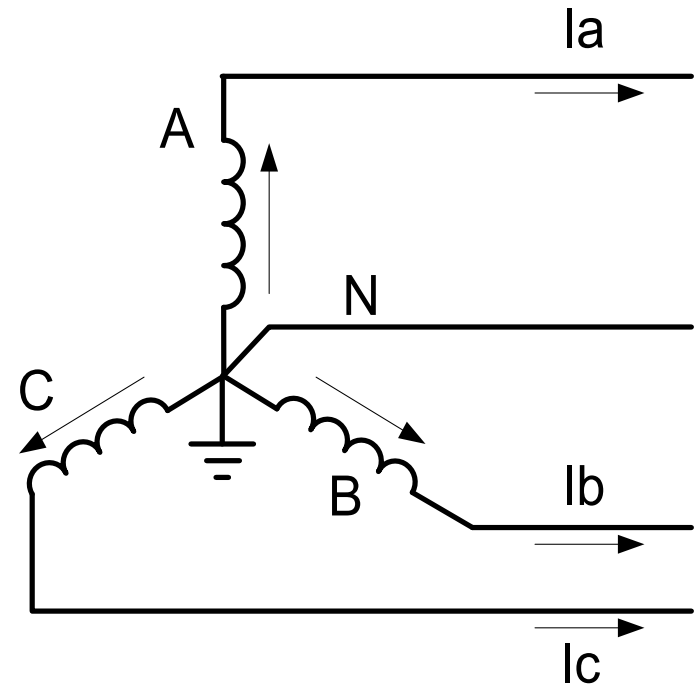
THREE PHASE POWER

PHASORS AND VECTOR NOTATION

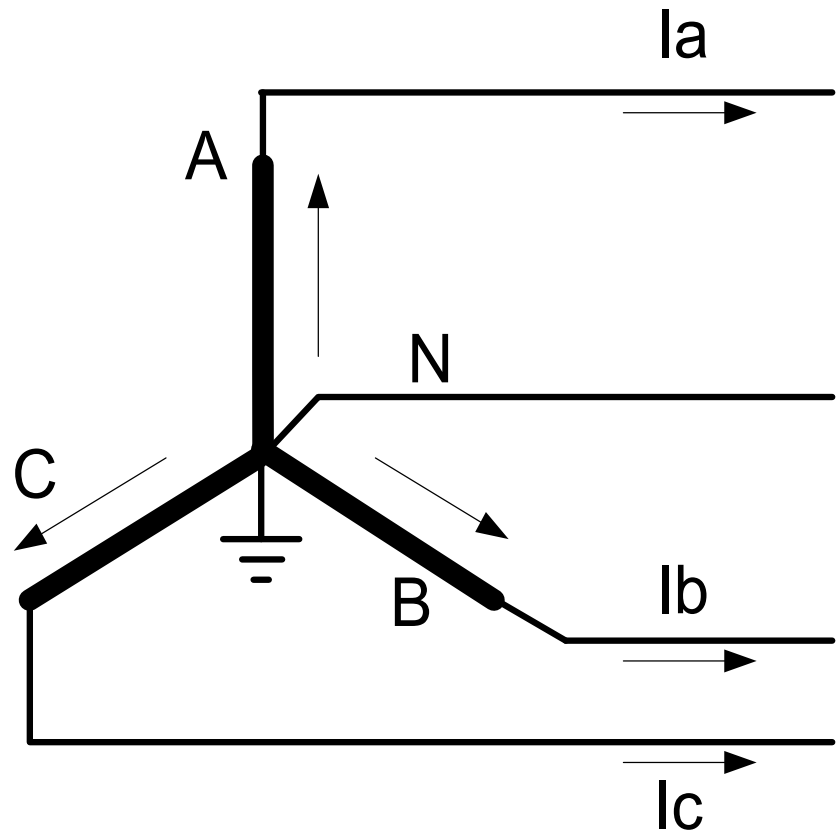
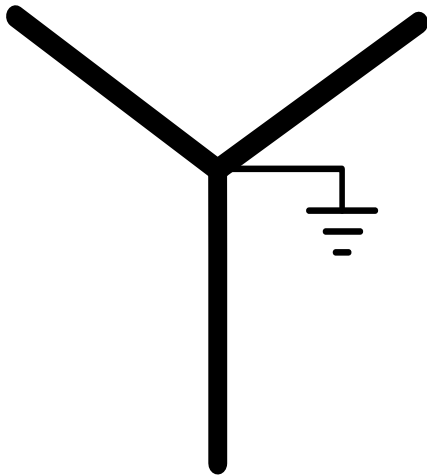
- The phasor diagram for a simple 3-phase system has three voltage phasors equally spaced at 120° intervals.
- Going clockwise the order is A – B – C.



- Systems formed by interconnecting secondary of 3 single phase transformers.
- Generally primaries are not shown unless details of actual transformer are being discussed.



- Often even the coils are not shown but are replaced by simple line drawings

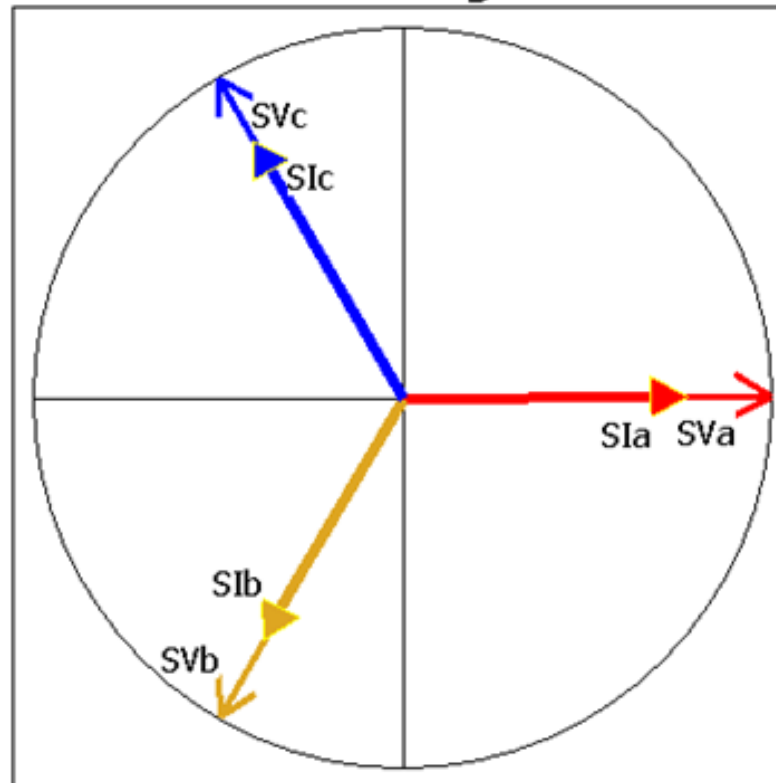


3 PHASE, 4-WIRE "Y" SERVICE

0° = UNITY POWER FACTOR

- Three Voltage Phasors
- 120° Apart
- Three Current Phasors
- Aligned with Voltage at PF=1

Vector Diagram



SVa	120.707	0.00°
SIa	1.012	359.97°
PF =	1.000	-0.03°
Lead		

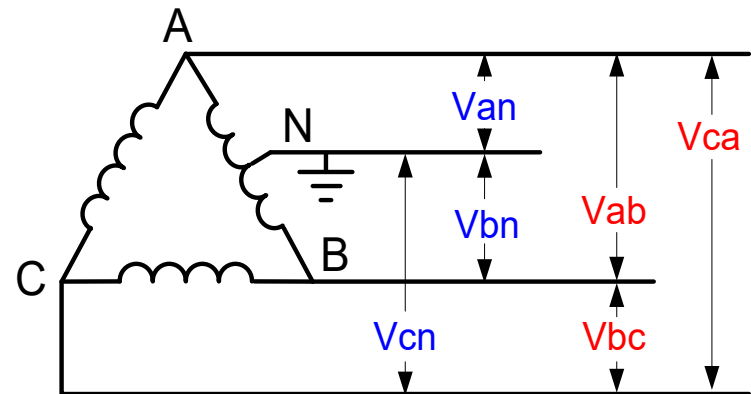
SVb	119.419	119.82°
SIb	0.994	119.70°
PF =	1.000	-0.12°
Lead		

SVc	119.727	239.94°
SIc	1.056	239.96°
PF =	1.000	0.02°
Lag		

Vsys =	119.951	
Isys =	1.021	
PF =	1.000	
ROT =	ABC	

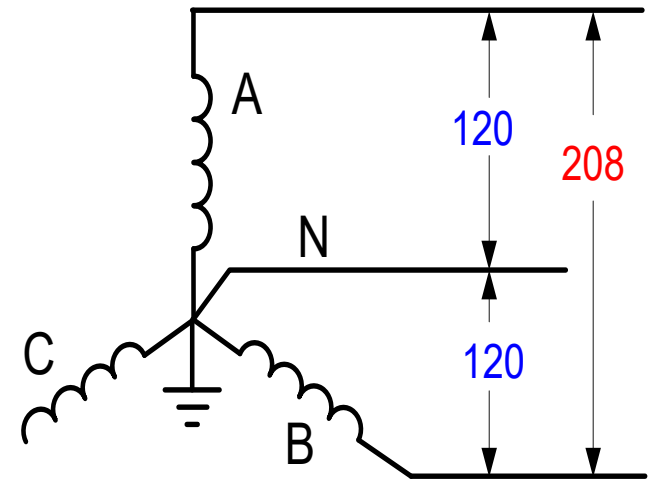
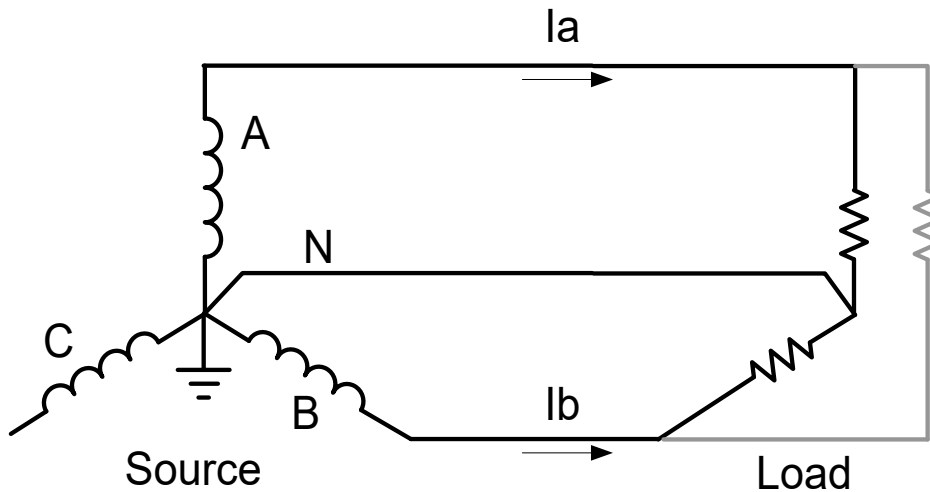
- Voltages are generally labeled V_a , V_b , V_c , V_n for the three phases and neutral
- This can be confusing in complex cases.
- The recommended approach is to use two subscripts so the two points between which the voltage is measured are unambiguous.

V_{ab} means voltage at “a” as measured relative to “b”.



2 PHASE, 3-WIRE "Y" SERVICE "NETWORK CONNECTION"

Single phase variant of the service.



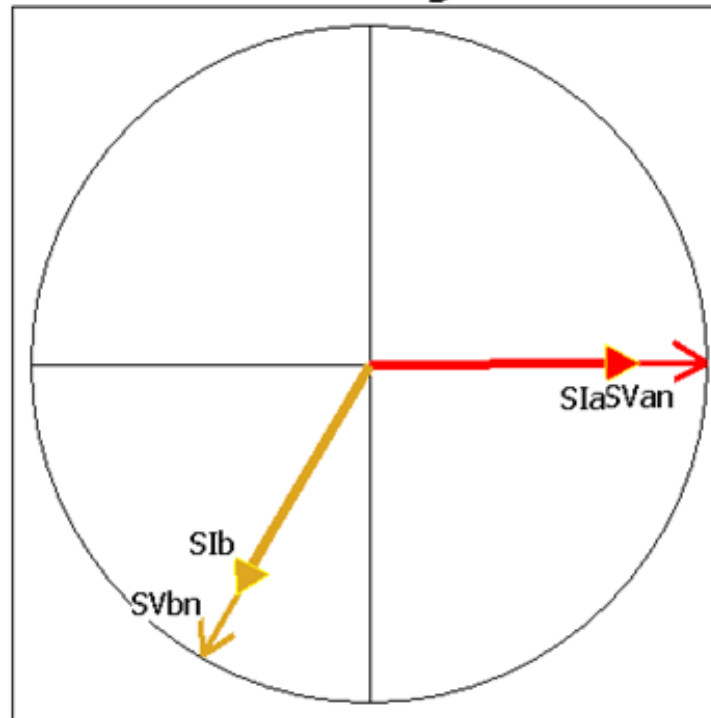
Two voltage sources with their returns connected to a common point.

Provides 208 rather than 240 volts across "high side" wires.

2 PHASE, 3-WIRE “NETWORK” SERVICE

- Two Voltage Phasors
- 120° Apart
- Two Current Phasors
- Aligned with Voltage at PF=1

Vector Diagram



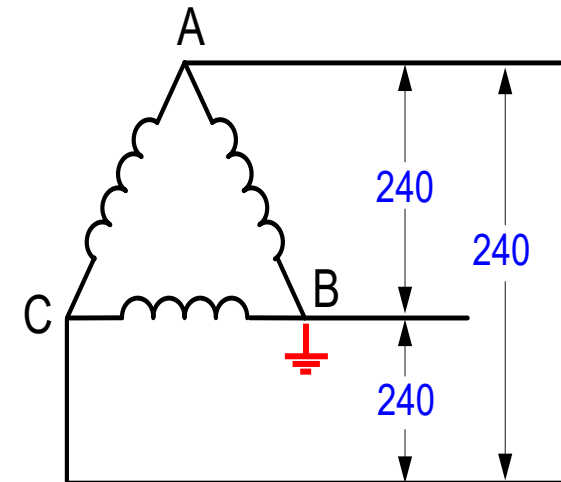
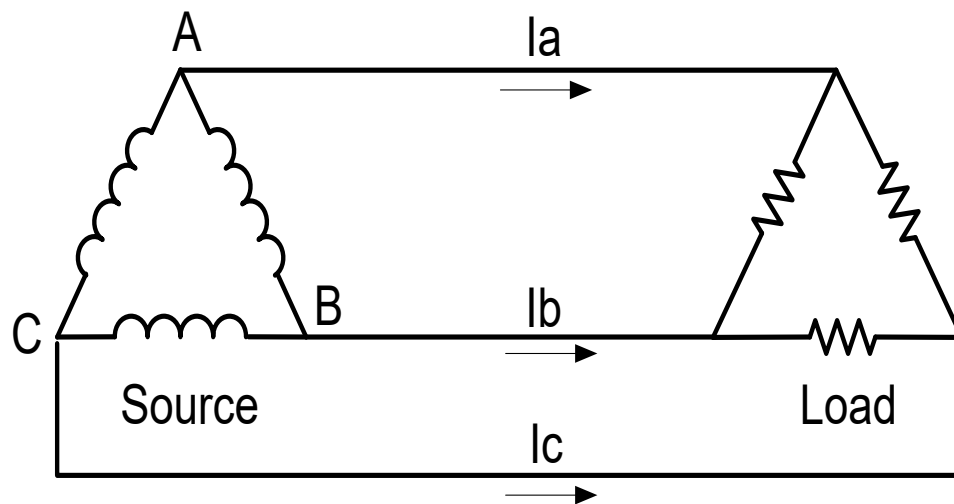
SVan	120.710	0.00°
SIa	1.012	359.99°
PF =	1.000	-0.01°
Lead		

SVbn	119.411	119.82°
SIb	0.993	119.72°
PF =	1.000	-0.09°
Lead		

Vsys =	120.060	
Isys =	1.003	
PF =	1.000	

3 PHASE, 3-WIRE DELTA SERVICE

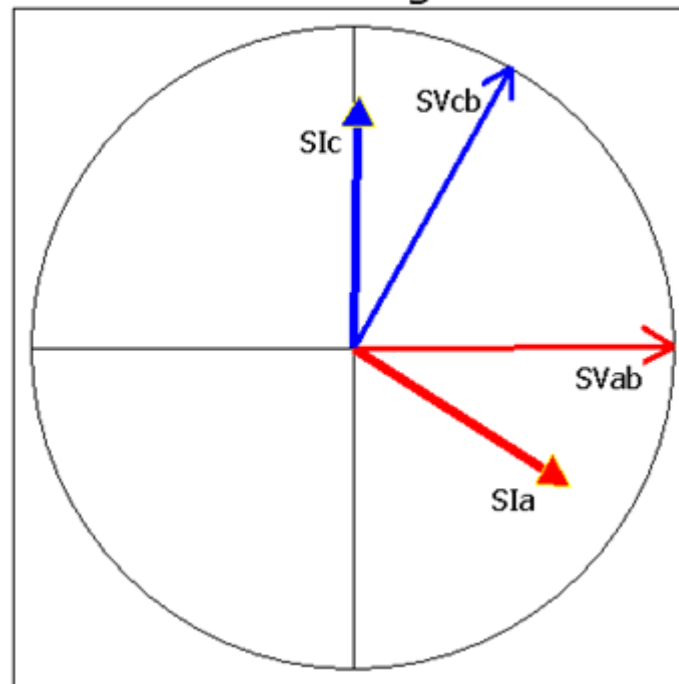
Common service type for industrial customers. This service may have NO neutral.



- Voltages normally measured relative to phase B.
 - Sometimes phase B will be grounded
- Voltage and current vectors do not align.
- Service is provided even when a phase is grounded.

- Two Voltage Phasors
- 60° Apart
- Two Current Phasors
- For a resistive load lags by 30°

Vector Diagram



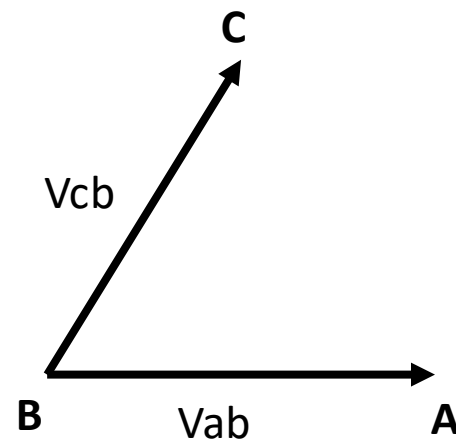
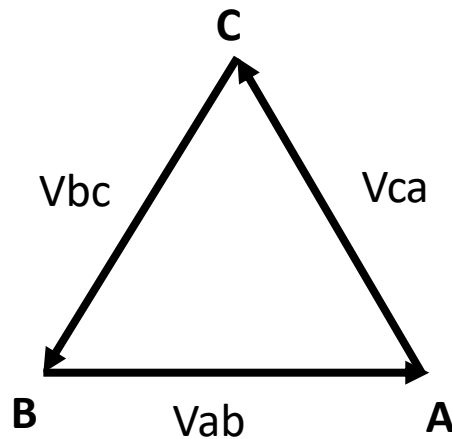
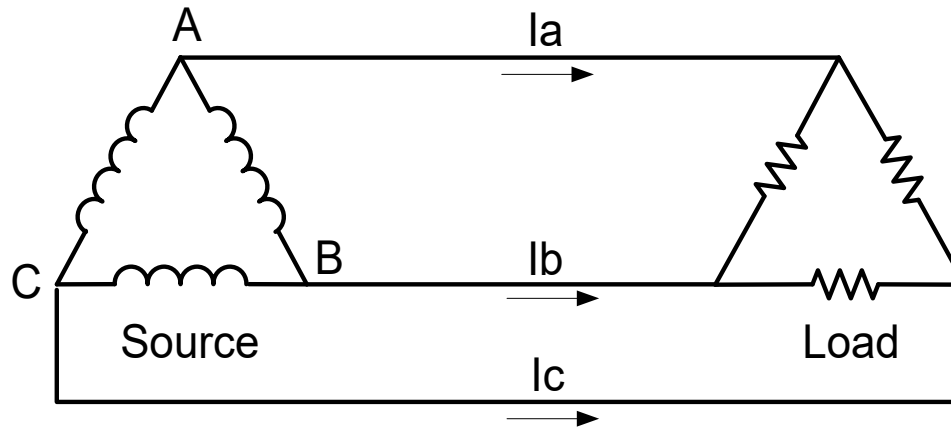
SVab	238.922	0.00°
SIa	1.055	32.74°
PF =	0.839	32.74°
Lag		

SVcb	237.914	299.48°
SIc	1.033	271.29°
PF =	0.881	-28.19°
Lead		

Vsys =	238.418
Isys =	1.044
PF =	0.860

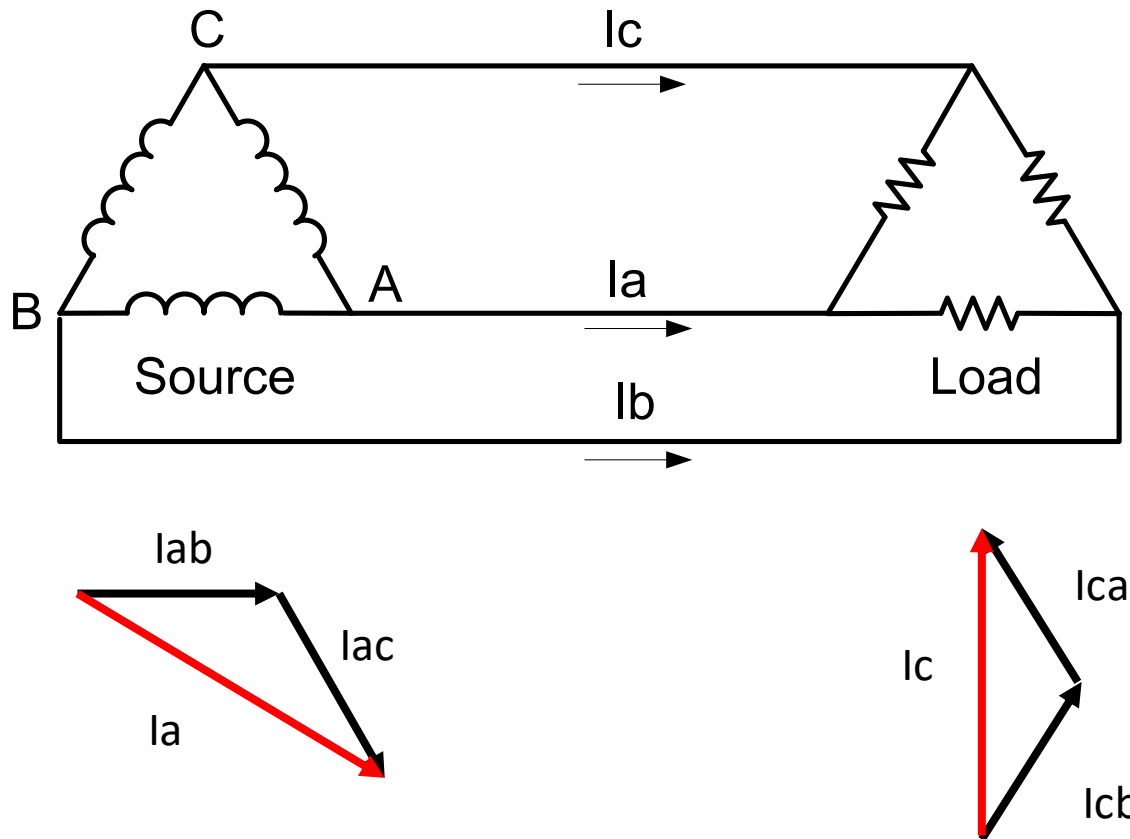
3 PHASE, 3-WIRE DELTA SERVICE

UNDERSTANDING THE DIAGRAM



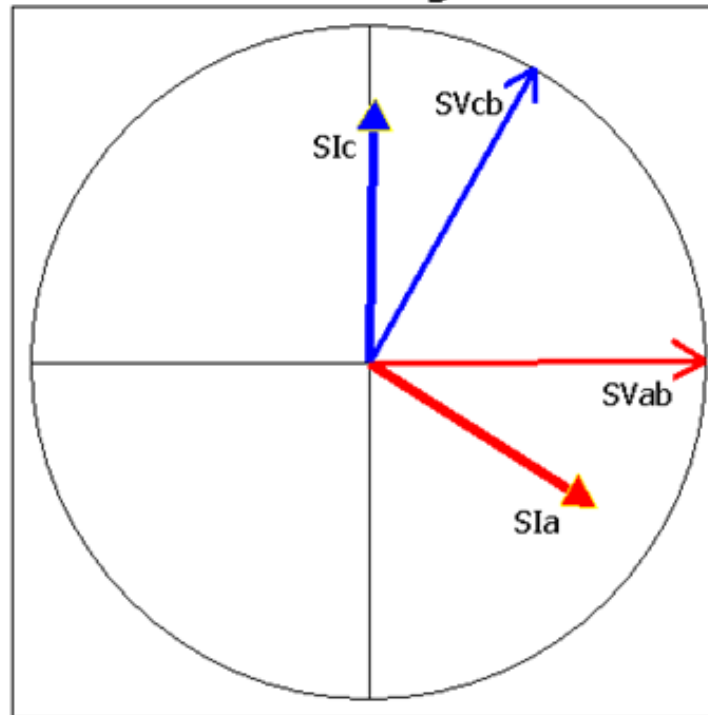
3 PHASE, 3-WIRE DELTA SERVICE

UNDERSTANDING THE DIAGRAM



- Two Voltage Phasors
- 60° Apart
- Two Current Phasors
- For a resistive load one current leads by 30° while the other lags by 30°

Vector Diagram



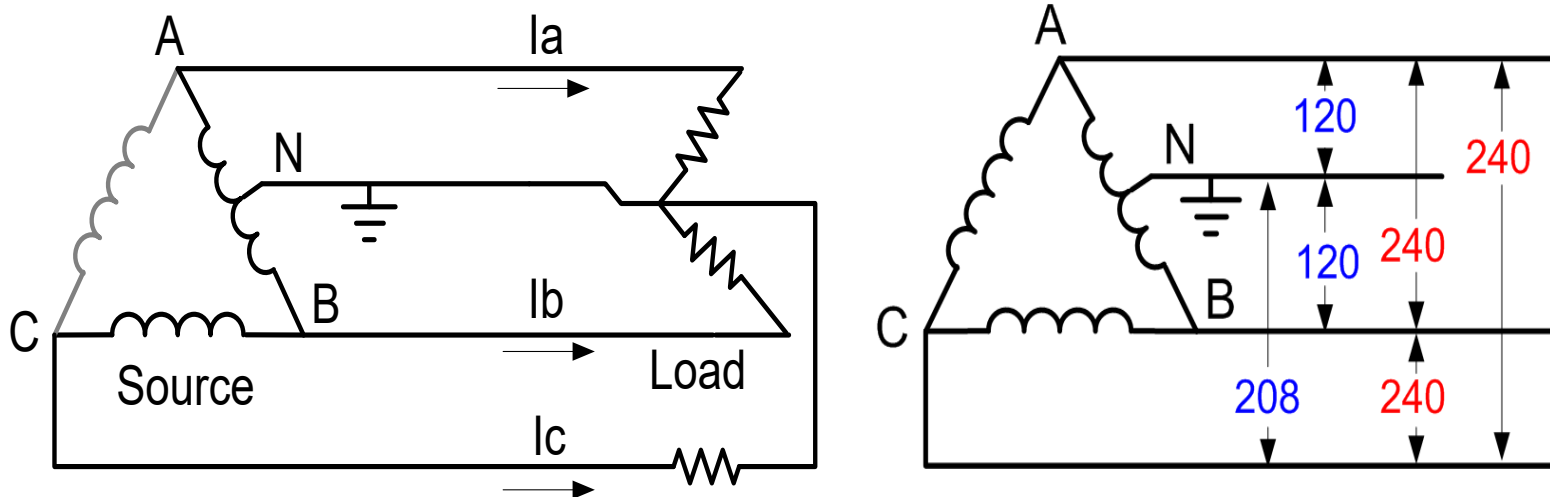
SVab	238.922	0.00°
SIa	1.055	32.74°
PF =	0.839	32.74°
Lag		

SVcb	237.914	299.48°
SIc	1.033	271.29°
PF =	0.881	-28.19°
Lead		

Vsys =	238.418	
Isys =	1.044	
PF =	0.860	

3 PHASE, 4-WIRE DELTA SERVICE

Common service type for industrial customers. Provides a residential like 120/240 service (lighting service) single phase 208 (high side) and even 3 phase 240 V.



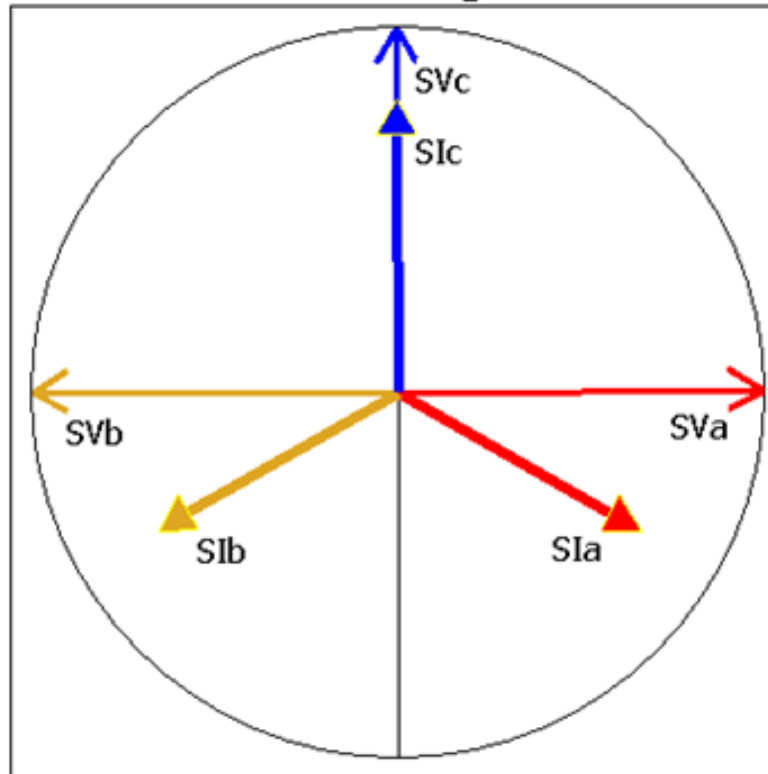
- Voltage phasors form a “T” 90° apart
- Currents are at 120° spacing
- In 120/120/208 form only the “hot” (208) leg has its voltage and current vectors aligned.

3 PHASE, 4-WIRE DELTA SERVICE

RESISTIVE LOAD

- Three Voltage Phasors
- 90° Apart
- Three Current Phasors
- 120° apart

Vector Diagram



SVa	120.684	0.00°
SIa	1.013	29.97°
PF =	0.866	29.97°
Lag		

SVb	119.439	179.81°
SIb	0.994	149.68°
PF =	0.865	-30.14°
Lead		

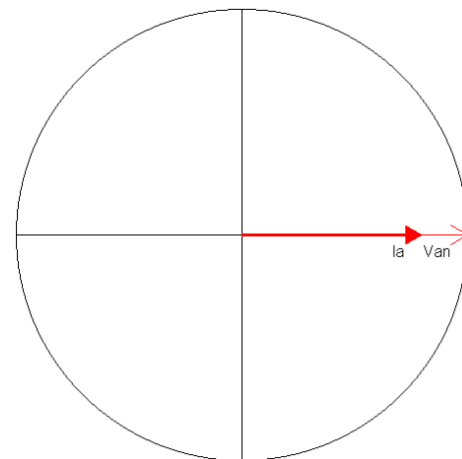
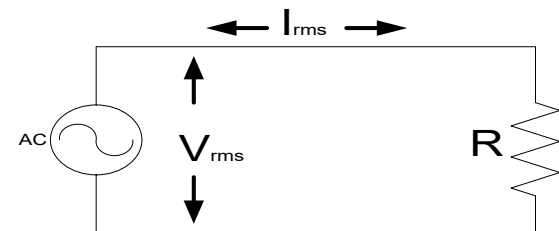
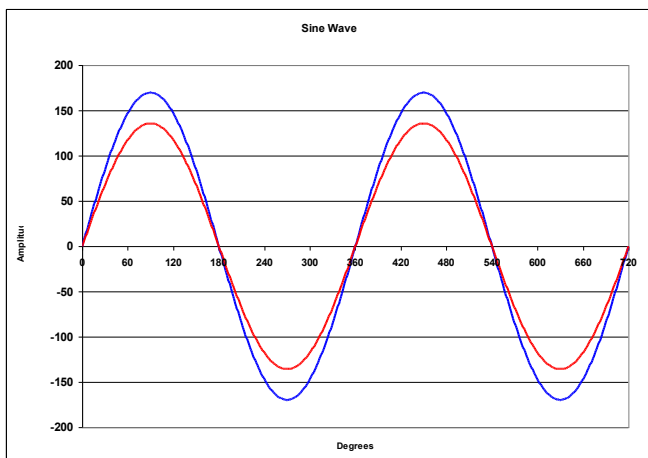
SVc	119.720	269.91°
SIc	1.056	269.97°
PF =	1.000	0.05°
Lag		

Vsys =	119.948	
Isys =	1.021	
PF =	0.910	
ROT =	ABC	



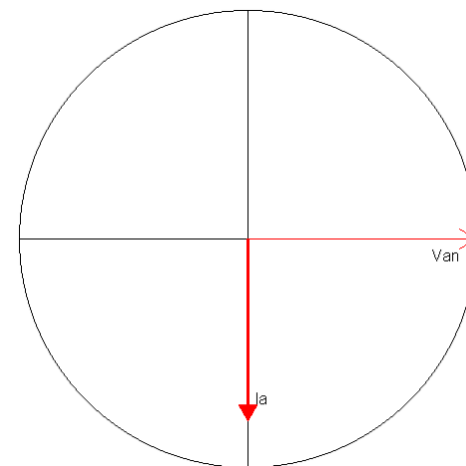
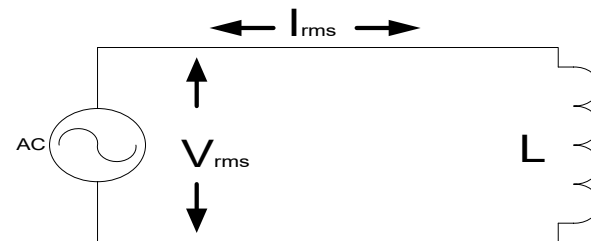
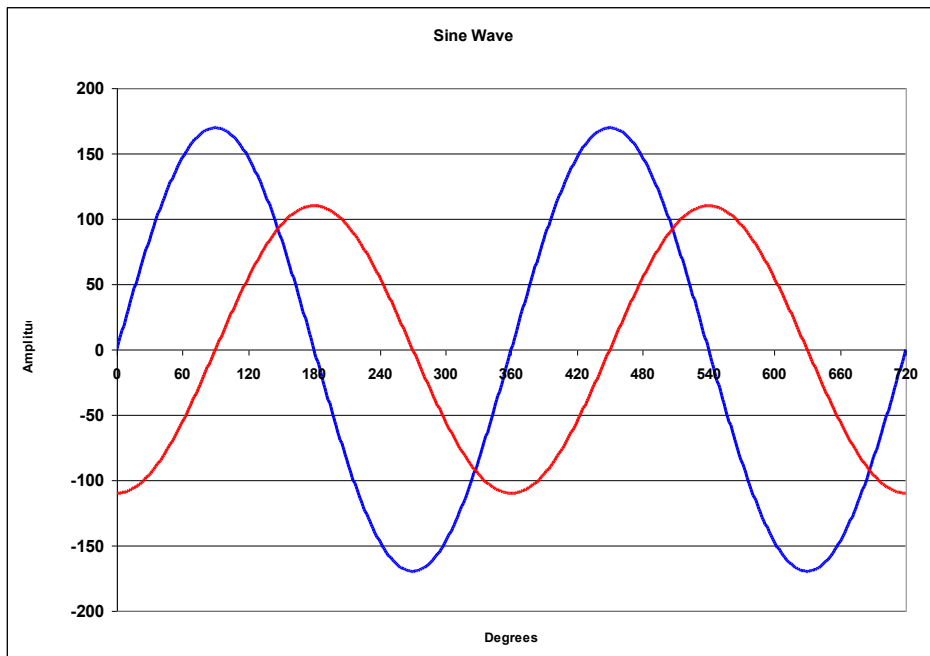
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AC THEORY – RESISTIVE LOAD



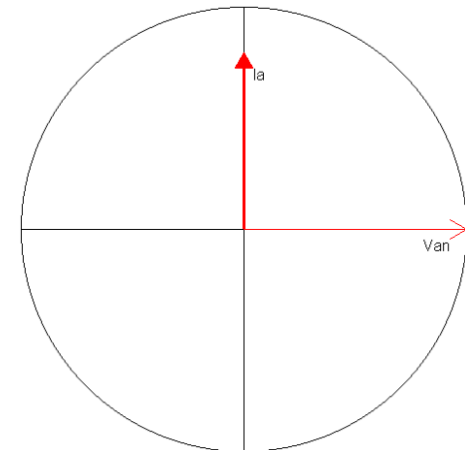
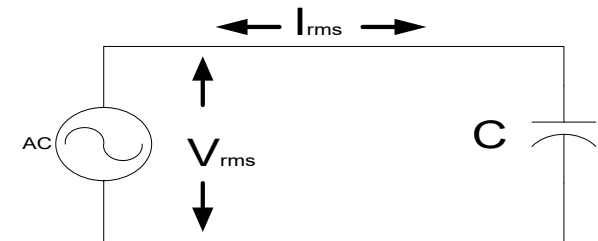
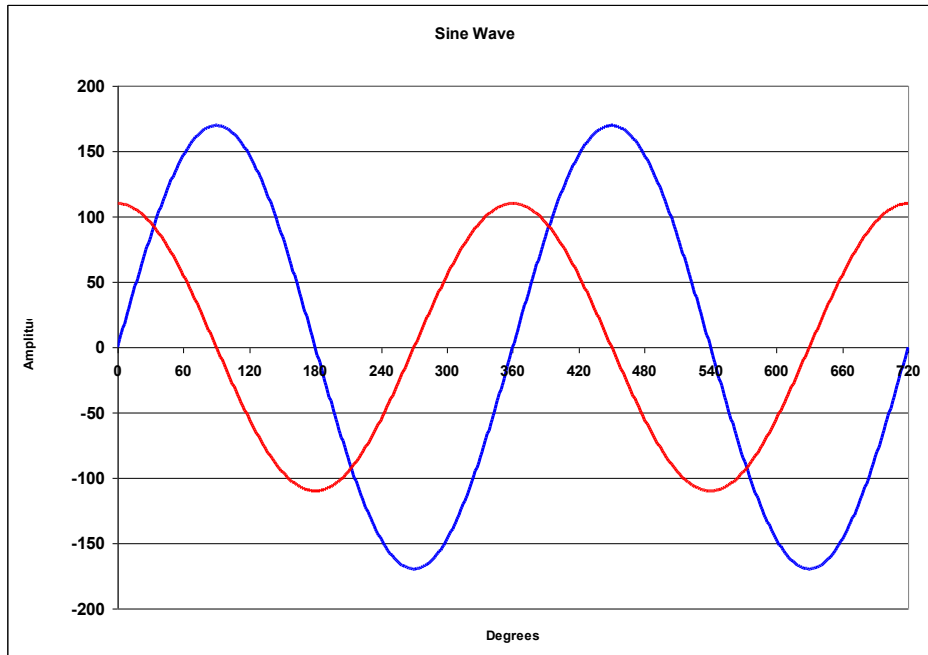
Resistors are measured in Ohms. When an AC voltage is applied to a resistor, the current is in phase. A resistive load is considered a “linear” load because when the voltage is sinusoidal the current is also sinusoidal.

AC THEORY – INDUCTIVE LOAD



Inductors are measured in Henries. When an AC voltage is applied to an inductor, the current is 90 degrees out of phase. We say the current “lags” the voltage. A inductive load is considered a “linear” load because when the voltage is sinusoidal the current is also sinusoidal.

AC THEORY – CAPACITIVE LOAD



Capacitors are measured in Farads. When an AC voltage is applied to a capacitor, the current is 90 degrees out of phase. We say the current “leads” the voltage. A capacitive load is considered a “linear” load because when the voltage is sinusoidal the current is sinusoidal.

- Power is defined as $P = VI$
- Since the voltage and current at every point in time for an AC signal is different, we have to distinguish between instantaneous power and average power. Generally when we say “power” we mean average power.
- Average power is only defined over an integral number of cycles.

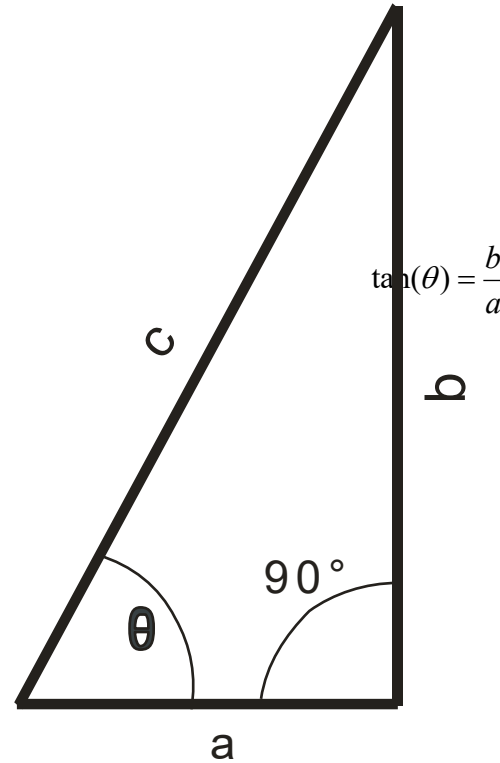
The Right Triangle:

The Pythagorean theory

$$c^2 = a^2 + b^2$$

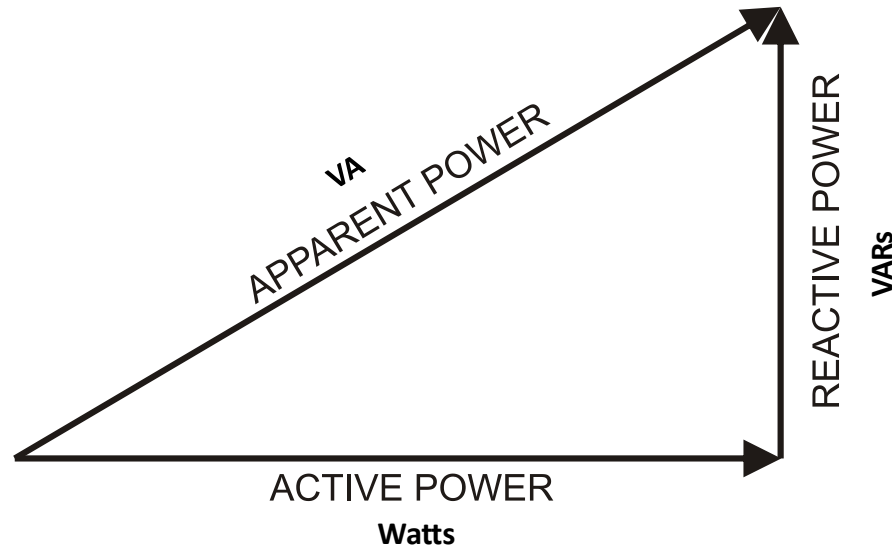
$$\sin(\theta) = \frac{b}{c}$$

$$\cos(\theta) = \frac{a}{c}$$



AC THEORY – POWER TRIANGLE

(SINUSOIDAL WAVEFORMS)

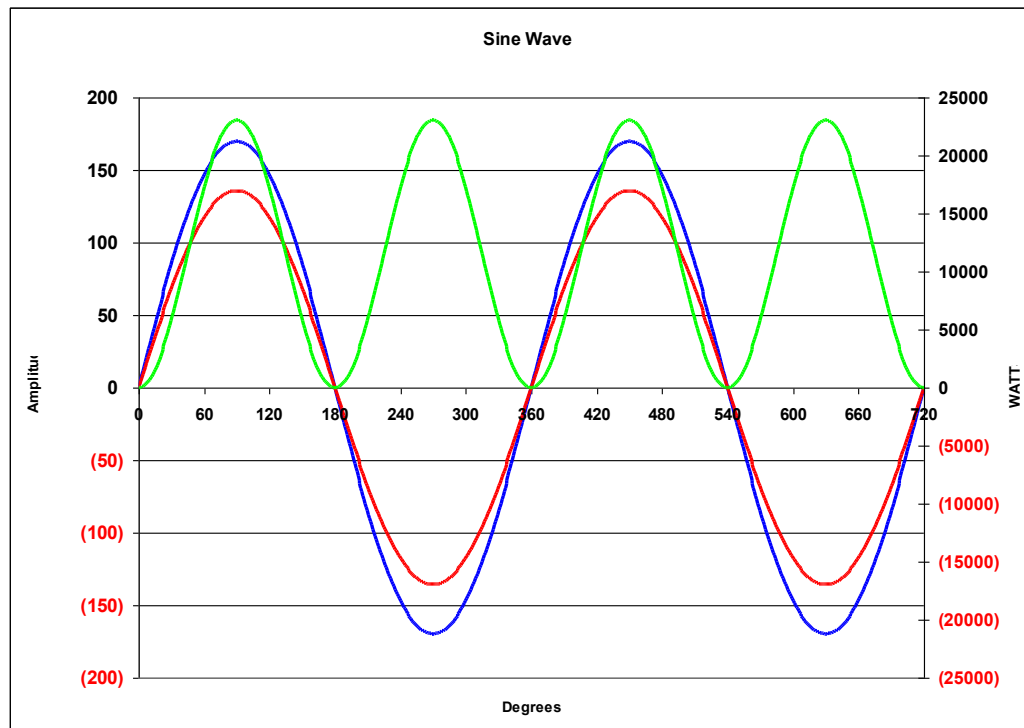


If $V = \sin(\omega t)$ and $I = \sin(\omega t - \theta)$ (the load is linear)
then

Active Power =	$VI \cos(\theta)$	Watts
Reactive Power =	$VI \sin(\theta)$	VARs
Apparent Power =	VI	VA
Power Factor =	$\text{Active/Apparent} = \cos(\theta)$	

For a resistive load:

$$p = vi = 2VI \sin^2(\omega t) = VI(1 - \cos(2\omega t))$$



$$V = 120\sqrt{2} \sin(2\pi ft)$$

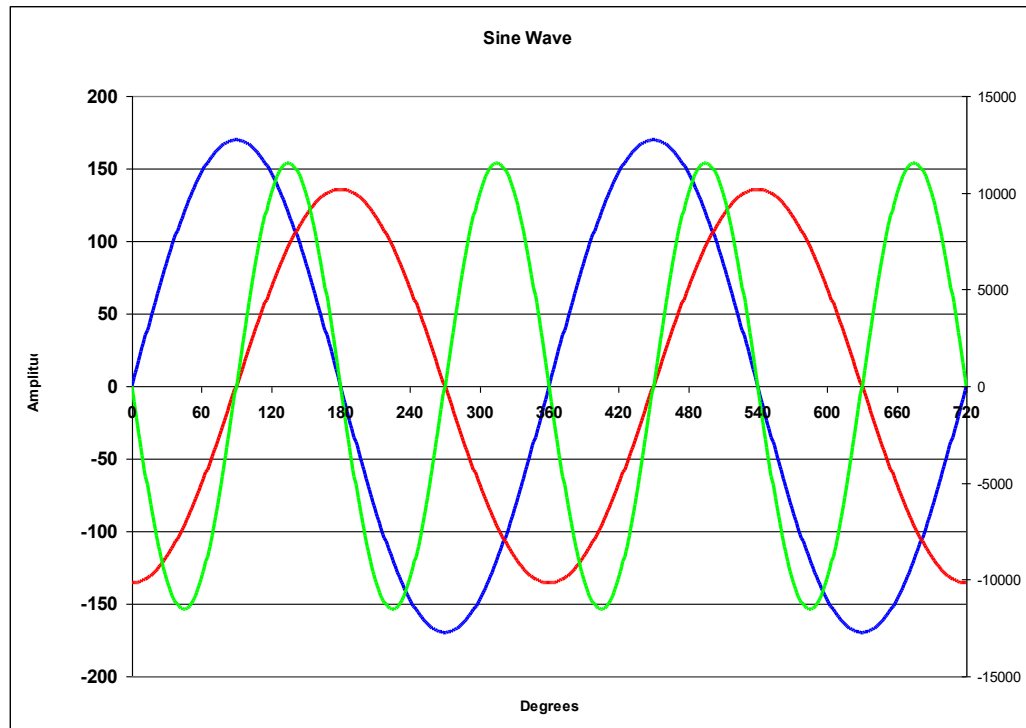
$$I = 96\sqrt{2} \sin(2\pi ft)$$

$$P = 23040 \sin^2(2\pi ft)$$

$$P = 11520 \text{ Watts}$$

For an inductive load:

$$p = vi = 2VI \sin(\omega t) \sin(\omega t - 90) = -VI \sin(2\omega t)$$



$$V = 120\sqrt{2} \sin(2\pi ft)$$

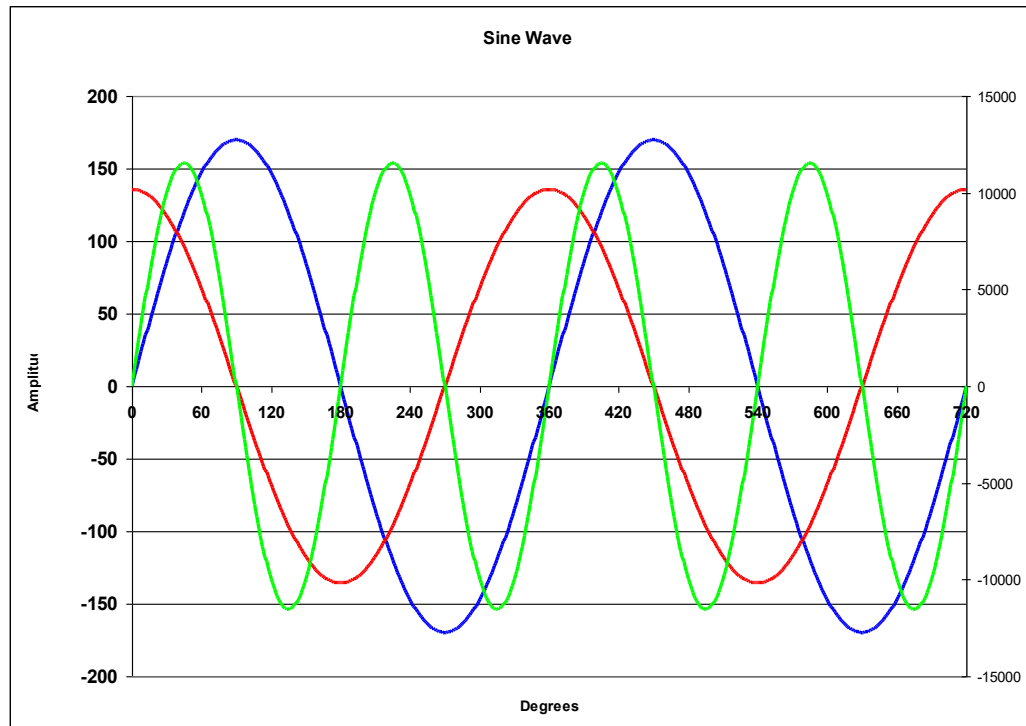
$$I = 96\sqrt{2} \sin(2\pi ft - 90)$$

$$P = -11520 \sin(2\pi ft)$$

$$P = 0 \text{ Watts}$$

For a capacitive load:

$$p = v i = 2VI \sin(\omega t) \sin(\omega t + 90) = VI \sin(2\omega t)$$



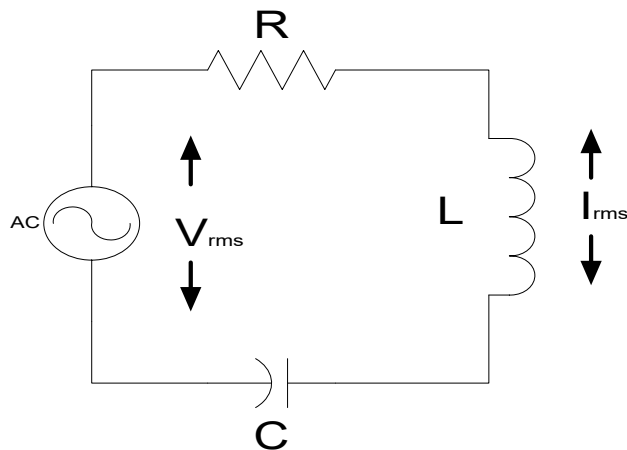
$$V = 120\sqrt{2} \sin(2\pi ft)$$

$$I = 96\sqrt{2} \sin(2\pi ft + 90)$$

$$P = 11520 \sin(2\pi ft)$$

P = 0 Watts

AC THEORY – COMPLEX CIRCUITS

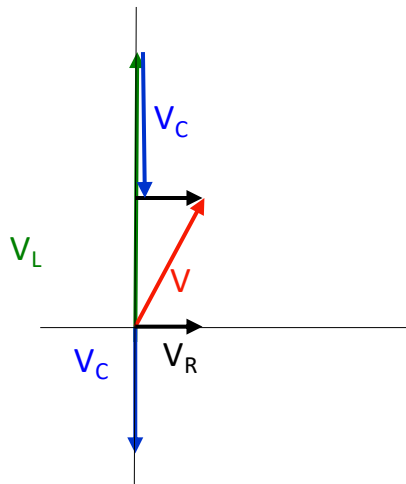


Amplitude (Current)

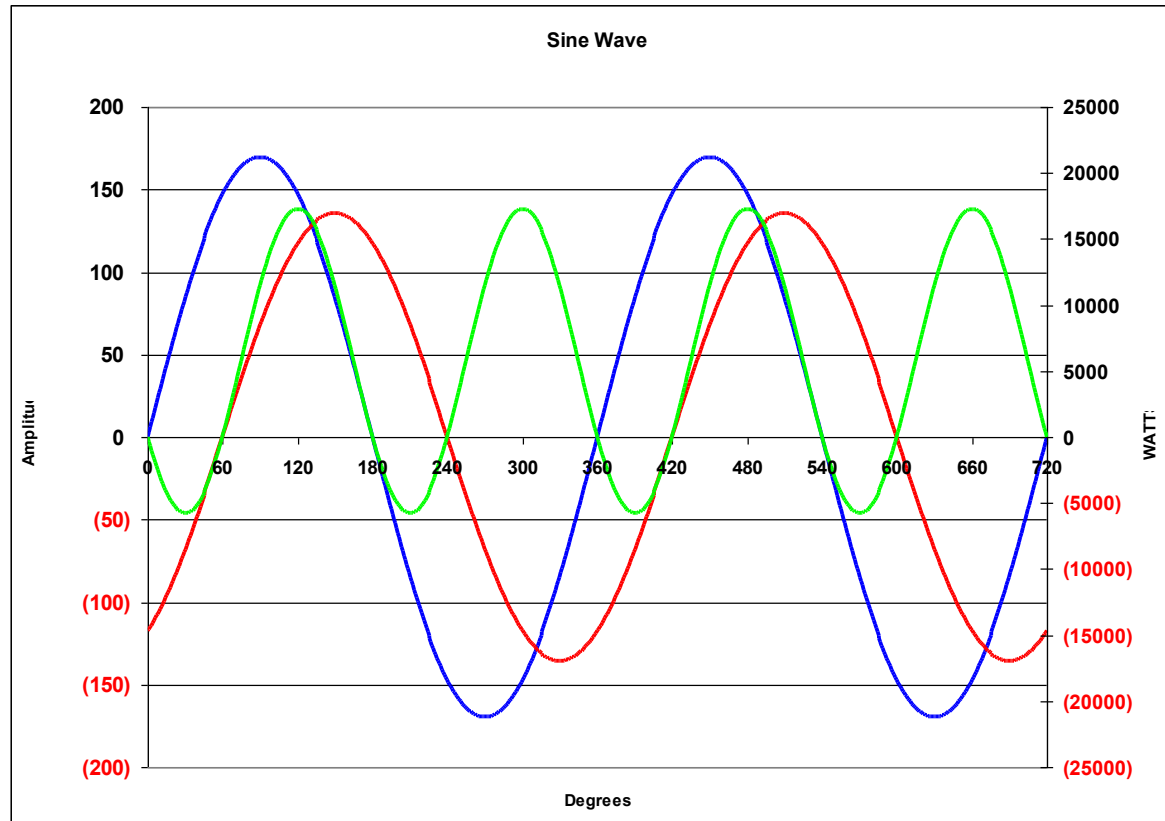
$$I = \frac{V}{\sqrt{R^2 + \left(\omega L - \frac{1}{\omega C}\right)^2}}$$

Phase (Current)

$$\varphi = \arctan \left[\frac{\left(\omega L - \frac{1}{\omega C}\right)}{R} \right]$$



AC THEORY – INSTANTANEOUS POWER



$$V = 120\sqrt{2} \sin(2\pi ft)$$

$$I = 96\sqrt{2} \sin(2\pi ft - 60^\circ)$$

$$P = VI = 23040(\cos(60^\circ) + \cos(4\pi ft - 60^\circ)) = 19953 - 23040 \cos(4\pi ft - 60^\circ)$$

If energy be supplied to any system of conductors through N wires, the total power in the system is given by the algebraic sum of the readings of N wattmeters, so arranged that each of the N wires contains one current coil, the corresponding voltage coil being connected between that wire and some common point. If this common point is on one of the N wires, the measurement may be made by the use of $N-1$ wattmeters.

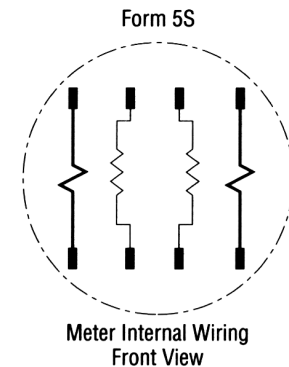
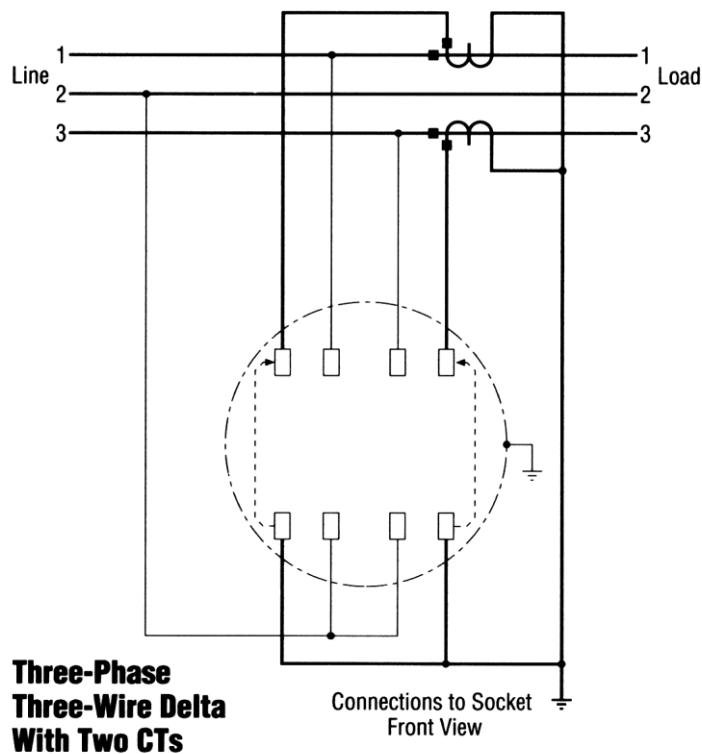
- Simply – We can measure the power in a N wire system by measuring the power in N-1 conductors.
- For example, in a 4-wire, 3-phase system we need to measure the power in 3 circuits.

- If a meter installation meets Blondel's Theorem then we will get accurate power measurements under all circumstances.
- If a metering system does not meet Blondel's Theorem then we will only get accurate measurements if certain assumptions are met.



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BLONDEL'S THEOREM



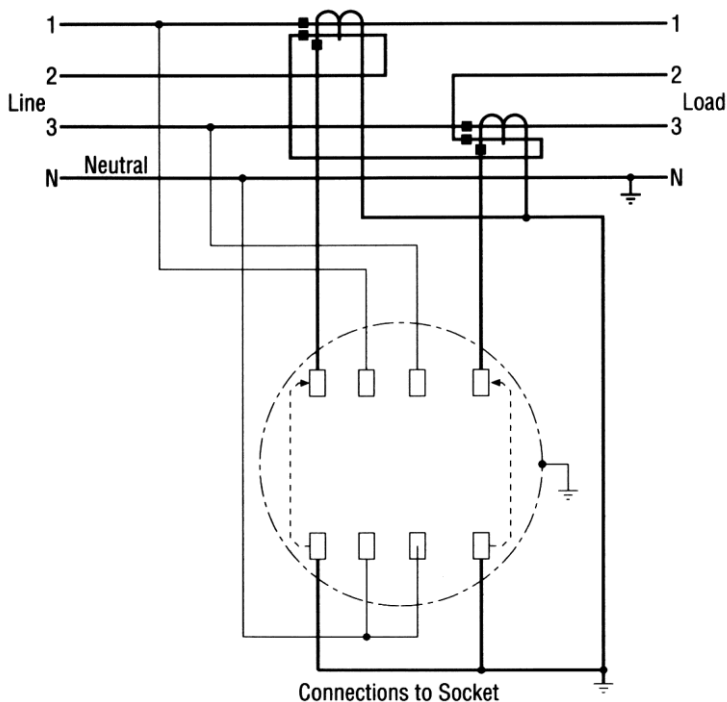
- Three wires
- Two voltage measurements with one side common to Line 2
- Current measurements on lines 1 & 3.

This satisfies Blondel's Theorem.

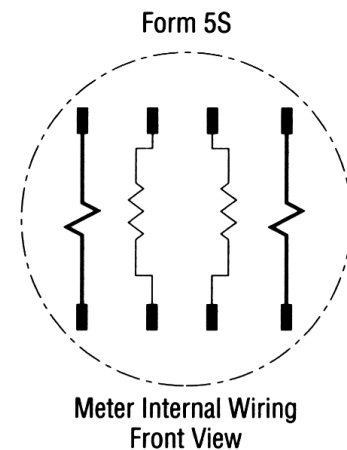


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BLONDEL'S THEOREM



**Three-Phase
Four-Wire Wye
With Two Equal-Ratio CTs**



- Four wires
- Two voltage measurements to neutral
- Current measurements on lines 1 & 3. How about line 2?

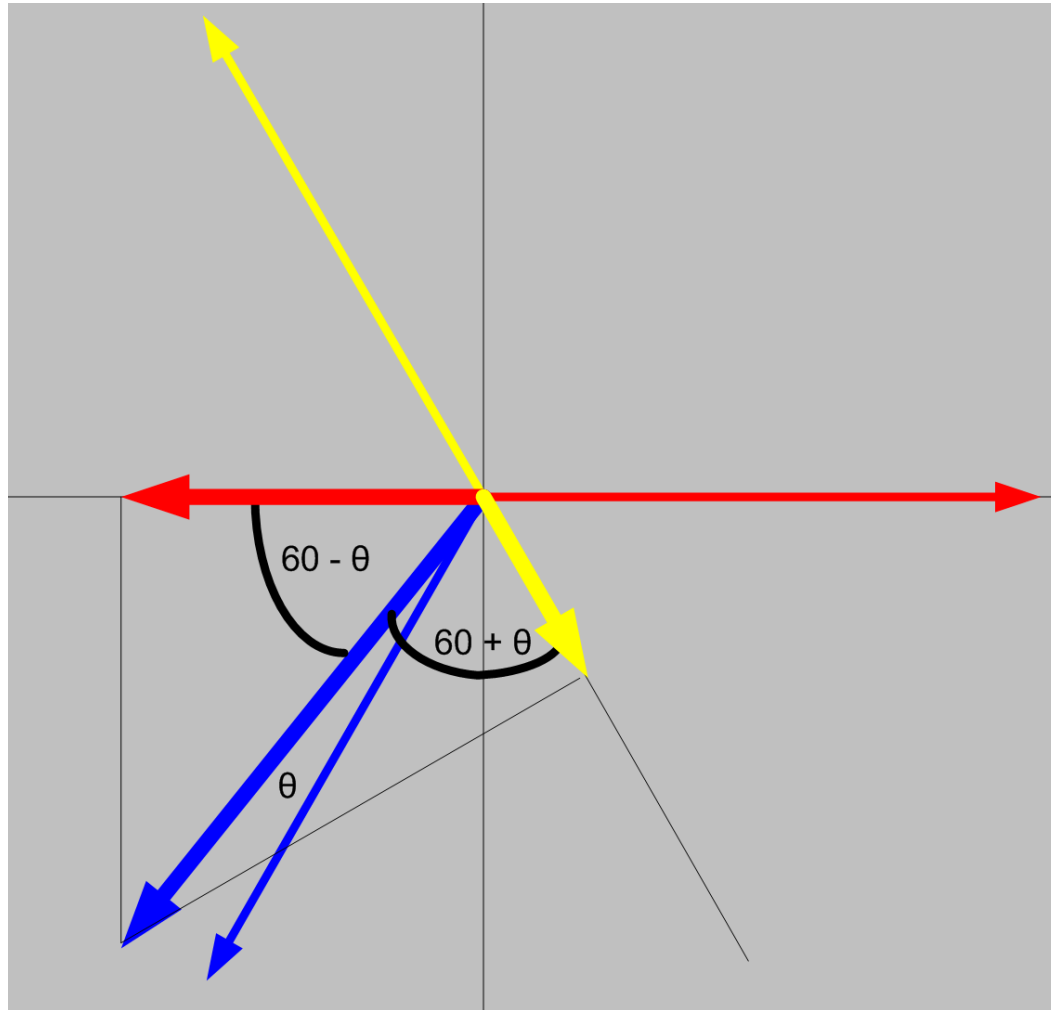
This DOES NOT satisfy Blondel's Theorem.

- In the previous example:
 - What are the “ASSUMPTIONS”?
 - When do we get errors?
- What would the “Right Answer” be?
- What did we measure?

$$P_{sys} = V_a I_a \cos(\theta_a) + V_b I_b \cos(\theta_b) + V_c I_c \cos(\theta_c)$$

$$P_{sys} = V_a [I_a \cos(\theta_a) - I_b \cos(\theta_b)] + V_c [I_c \cos(\theta_c) - I_b \cos(\theta_b)]$$

BLONDEL'S THEOREM



- Phase B power would be:
 - $P = V_b I_b \cos\theta$
- But we aren't measuring V_b
- What we are measuring is:
 - $I_b V_a \cos(60^\circ - \theta) + I_b V_c \cos(60^\circ + \theta)$
- $\cos(\alpha + \beta) = \cos(\alpha)\cos(\beta) - \sin(\alpha)\sin(\beta)$
- $\cos(\alpha - \beta) = \cos(\alpha)\cos(\beta) + \sin(\alpha)\sin(\beta)$
- So

- $P_b = I_b V_a \cos(60^\circ - \theta) + I_b V_c \cos(60^\circ + \theta)$
- Applying the trig identity
 - $I_b V_a (\cos(60^\circ)\cos(\theta) + \sin(60^\circ)\sin(\theta))$
 $I_b V_c (\cos(60^\circ)\cos(\theta) - \sin(60^\circ)\sin(\theta))$
 - $I_b (V_a + V_c) 0.5 \cos(\theta) + I_b (V_c - V_a) 0.866 \sin(\theta)$
- Assuming
 - Assume $V_b = V_a = V_c$
 - And, they are exactly 120° apart
- $P_b = I_b (2V_b) (0.5 \cos \theta) = I_b V_b \cos \theta$

- If $V_a \neq V_b \neq V_c$ then the error is
- %Error =
$$-I_b \left\{ (V_a + V_c) / (2V_b) - (V_a - V_c) 0.866 \sin(\theta) / (V_b \cos(\theta)) \right\}$$

How big is this in reality? If

$V_a=117, V_b=120, V_c=119, PF=1$ then $E=-1.67\%$

$V_a=117, V_b=116, V_c=119, PF=.866$ then $E=-1.67\%$

Power Measurements Handbook

Condition	% V	% I	Phase A				Phase B				non-Blondel
			V	ϕ_{van}	I	ϕ_{ian}	V	ϕ_{vbn}	I	ϕ_{ibn}	% Err
	Imb	Imb									
All balanced	0	0	120	0	100	0	120	180	100	180	0.00%
Unbalanced voltages PF=1	18%	0%	108	0	100	0	132	180	100	180	0.00%
Unbalanced current PF=1	0%	18%	120	0	90	0	120	180	110	180	0.00%
Unbalanced V&I PF=1	5%	18%	117	0	90	0	123	180	110	180	-0.25%
Unbalanced V&I PF=1	8%	18%	110	0	90	0	120	180	110	180	-0.43%
Unbalanced V&I PF=1	8%	50%	110	0	50	0	120	180	100	180	-1.43%
Unbalanced V&I PF=1	18%	40%	108	0	75	0	132	180	125	180	-2.44%
Unbalanced voltages PF \neq 1 PF _a = PF _b	18%	0%	108	0	100	30	132	180	100	210	0.00%
Unbalanced current PF \neq 1 PF _a = PF _b	0%	18%	120	0	90	30	120	180	110	210	0.00%
Unbalanced V&I PF \neq 1 PF _a = PF _b	18%	18%	108	0	90	30	132	180	110	210	-0.99%
Unbalanced V&I PF \neq 1 PF _a = PF _b	18%	40%	108	0	75	30	132	180	125	210	-2.44%
Unbalanced voltages PF \neq 1 PF _a \neq PF _b	18%	0%	108	0	100	60	132	180	100	210	-2.61%
Unbalanced current PF \neq 1 PF _a \neq PF _b	0%	18%	120	0	90	60	120	180	110	210	0.00%
Unbalanced V&I PF \neq 1 PF _a \neq PF _b	18%	18%	108	0	90	60	132	180	110	210	-3.46%
Unbalanced V&I PF \neq 1 PF _a \neq PF _b	18%	40%	108	0	75	60	132	180	125	210	-4.63%

- Power is defined as $P = VI$
- Since the voltage and current at every point in time for an AC signal is different, we have to distinguish between instantaneous power and average power. Generally when we say “power” we mean average power.
- Average power is only defined over an integer number of cycles.

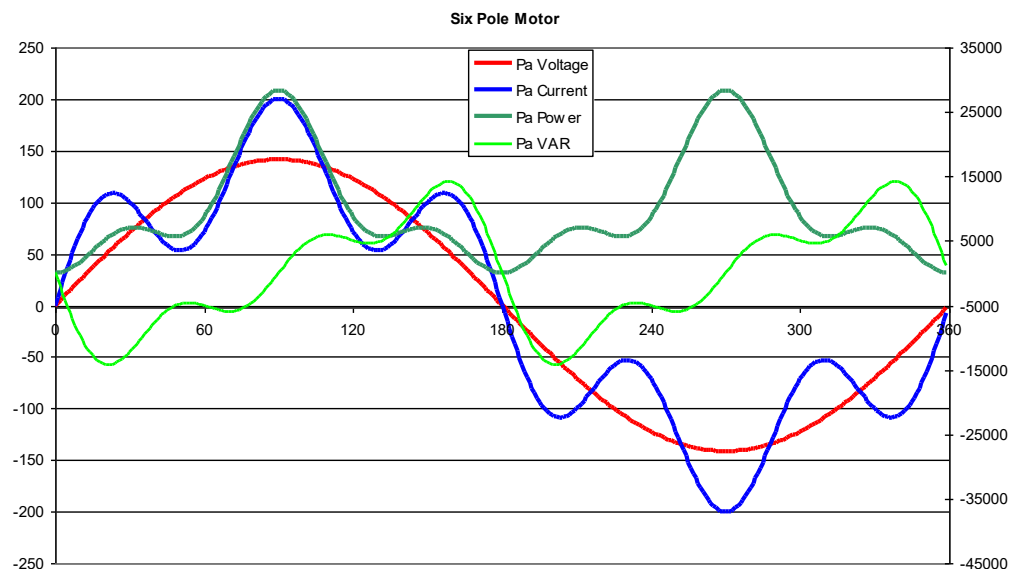
- Every thing discussed so far was based on “Linear” loads.
 - For linear loads the current is always a simple sine wave. Everything we have discussed is true.
- For nearly a century after AC power was in use ALL loads were linear.
- Today, many loads are NON-LINEAR.



TESCO METERING

HARMONIC LOAD WAVEFORM

Eq.#	Quantity	Phase A
1	V(rms) (Direct Sum)	100
2	I(rms) (Direct Sum)	108
3	V(rms) (Fourier)	100
4	I(rms) (Fourier)	108
5	$P_a = (\int V(t)I(t)dt)$	10000
6	$P_b = \frac{1}{2}\sum V_n I_n \cos(\theta)$	10000
7	$Q = \frac{1}{2}\sum V_n I_n \sin(\theta)$	0.000
8	$S_a = \text{Sqrt}(P^2 + Q^2)$	10000
9	$S_b = V_{rms} * I_{rms}(DS)$	10833
10	$S_c = V_{rms} * I_{rms}(F)$	10833
13	$PF = P_a / S_a$	1.000
14	$PF = P_b / S_b$	0.923
15	$PF = P_b / S_c$	0.923



$$V = 100\sin(\omega t) \quad I = 100\sin(\omega t) + 42\sin(5 \omega t)$$

HARMONIC LOAD WAVEFORM

Eq.#	Quantity	Phase A
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7	$Q = \frac{1}{2} \sum V_n I_n \sin(\theta)$	0.000
8	$S_a = \sqrt{P^2 + Q^2}$	10000
9	$S_b = V_{rms} * I_{rms}(DS)$	10833
10	$S_c = V_{rms} * I_{rms}(F)$	10833
13	$PF = P_a / S_a$	1.000
14	$PF = P_b / S_b$	0.923
15	$PF = P_b / S_c$	0.923

- Important things to note:

- Because the voltage is NOT distorted, the harmonic in the current does not contribute to active power.
- It does contribute to the Apparent power.
- Does the Power Triangle hold

$$S ? = \sqrt{P^2 + Q^2}$$

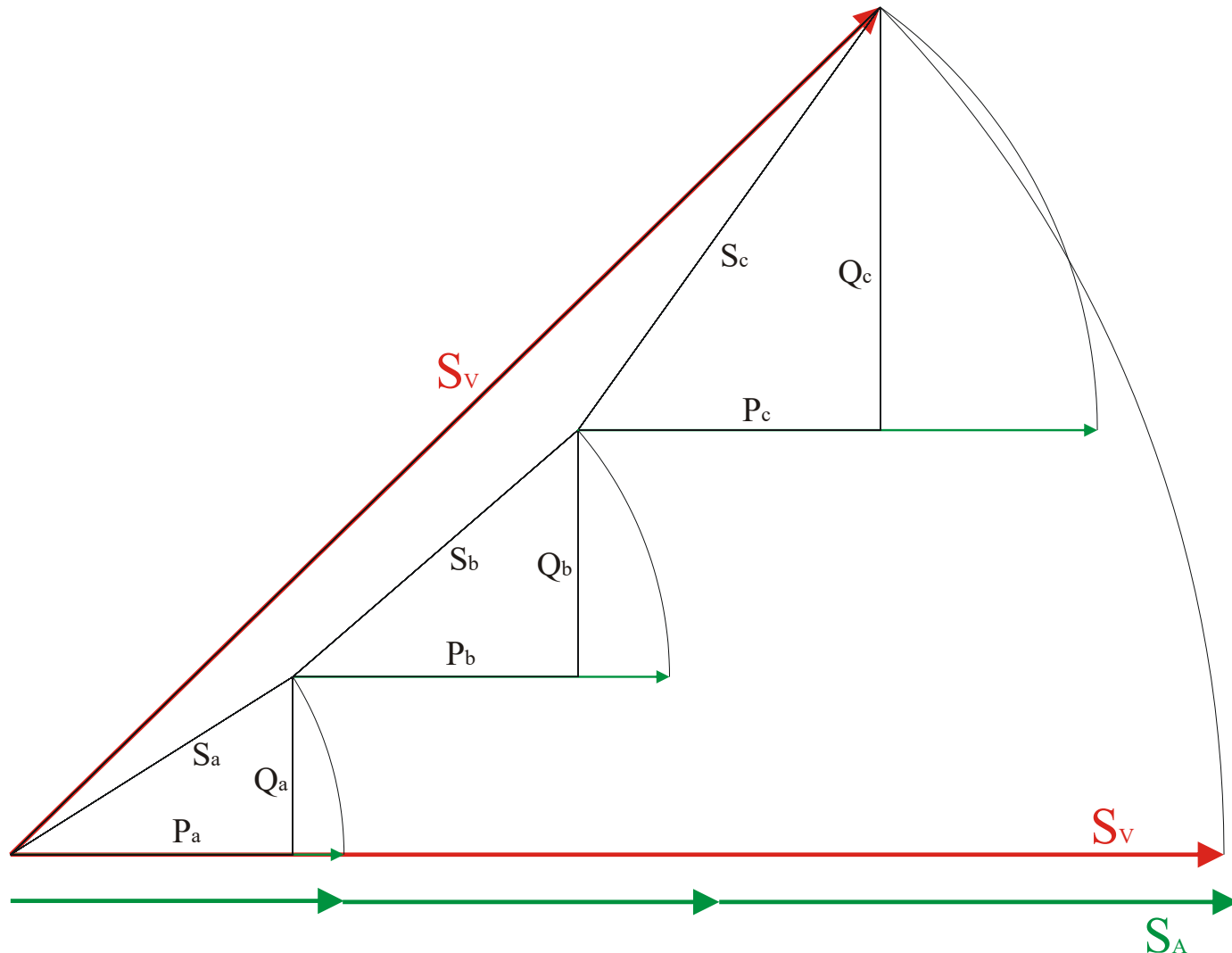
- There is considerable disagreement about the definition of various power quantities when harmonics are present.

$$V = 100\sin(\omega t) \quad I = 100\sin(\omega t) + 42\sin(5 \omega t)$$

3 PHASE POWER MEASUREMENT

- We have discussed how to measure and view power quantities (W, VARs, VA) in a single phase case.
- How do we combine them in a multi-phase system?
- Two common approaches:
 - Arithmetic
 - Vectorial

3 PHASE POWER MEASUREMENT

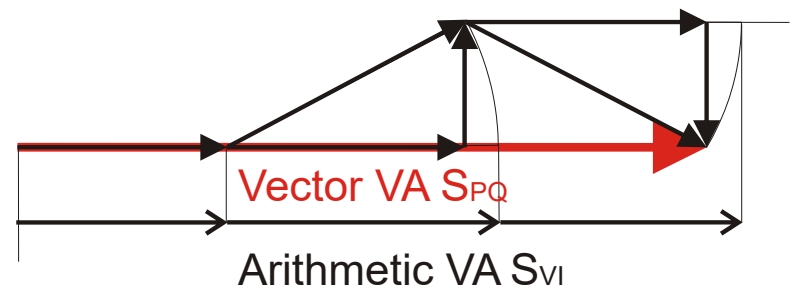


3 PHASE POWER MEASUREMENT

- VAR and VA calculations can lead to some strange results:
 - If we define

$$VA = \sqrt{(W_A + W_B + W_C)^2 + (Q_A + Q_B + Q_C)^2}$$

PH	W	Q	VA
A	100	0	100
B	120	55	132
C	120	-55	132
Arithmetic VA			364
Vector VA			340





Pete Brown

TSTM

This presentation can also be found under Meter Conferences and Schools on the TESCO website: tescometering.com

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