Test Switch Operations and Accessories

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CARIBBEAN METER SCHOOL

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ATLANTA, GA

Purpose:

To acquaint the attendees with the use and purpose of Meter Test Switches

Course Breakdown of Topics:

- **Using Test Switches**
- **Meter Test Switch Specifications**
- **Meter Test Switch Configurations**
- **Meter Test Switch Accessories**
- **Pre-Wired Transformer Rated Enclosures**

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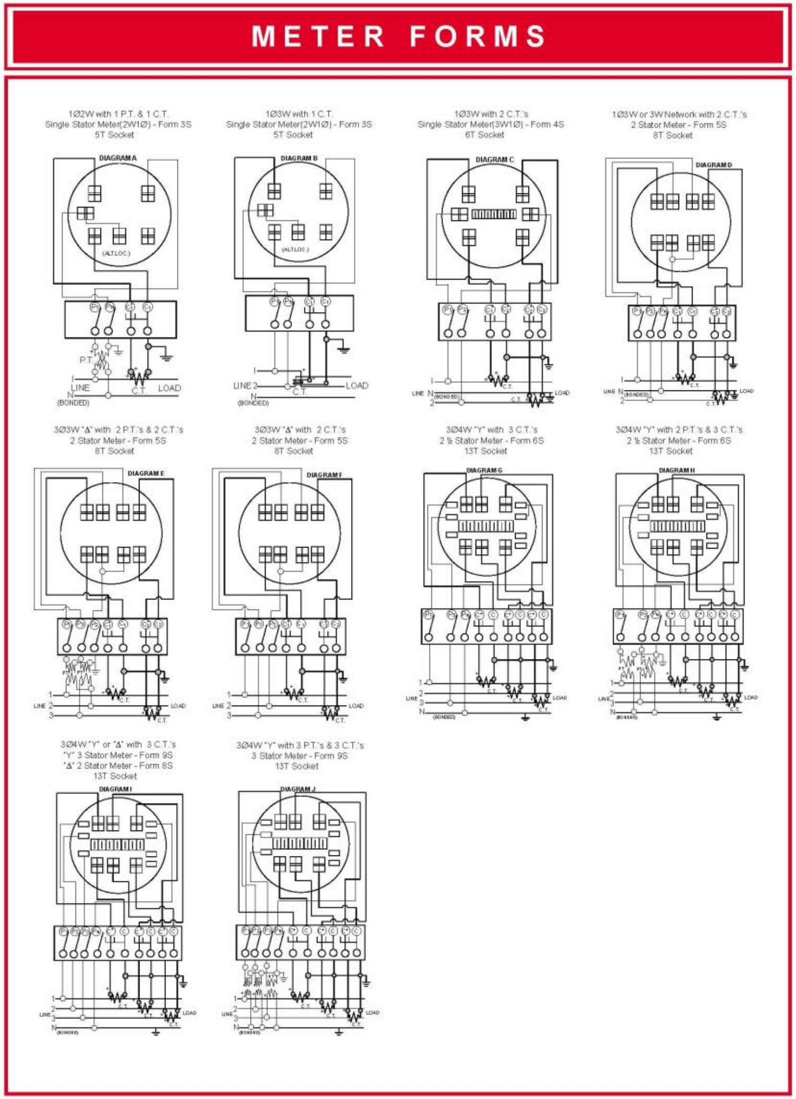
SAFETY

- Testing current transformers while they are in service can be a dangerous operation if certain safety procedures are not followed. The secondary loop of a current transformer must NEVER BE OPENED when service current is present in the primary. When there is current in the primary, and the secondary of a current transformer is open circuited, the voltage across the secondary can rise to hundreds and even thousands of volts, creating an extremely dangerous situation. The open CT secondary voltage magnitude varies with CT design and primary current flow. The high voltage that is present on the open secondary of an energized current transformer generates two great hazards. The first hazard is ELECTRICAL SHOCK TO TESTING PERSONNEL. The second hazard is THE BREAKDOWN OF THE CURRENT TRANSFORMER INSULATION. Both hazards can be avoided provided that the secondary of the current transformer is never opened. The safest current transformer installations for testing are those that have a Test Switch as part of the secondary loop. A Test Switch is a device that will facilitate inserting instrumentation in the current transformer secondary loop without the danger of opening the circuit.

Typical Connections for Common Meter Forms



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Test Switch Specifications

- ANSI C12 Definitions
- Test Switch Materials
- Plating
- Barriers
- Wiring Connections
- What to look for
- Covers

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ANSI C12.9 TEST SWITCH DEFINITIONS

For Test Switches and Jacks for Transformer-Rated Meters

1 Scope

This standard is intended to encompass the dimensions and functions of meter test switches used with transformer-rated watthour meters in conjunction with instrument transformers and test plugs used in conjunction with the test switch.

2 Definitions

2.1 short-circuiting switch

A single-pole double-throw (make-before-break) transfer switch used to transfer current away from the meter.

2.2 test jack

A spring-jaw receptacle in the current element of a test switch that provides a bipolar test connection in the metering current circuit without interruption of the current circuit.

2.3 test jack switch

A single-pole single-throw disconnect switch used in conjunction with a test jack to provide a parallel current path during normal operating conditions.

2.4 test plug

A bipolar mating plug to a test jack for inserting instrumentation into the metering current circuit.

2.5 voltage switch

A single-pole single-throw switch used to open or close a voltage circuit.

3 Standard ratings

3.1 Current

The current rating shall be 20 A minimum.

3.2 Voltage

The voltage rating shall be 300 V or 600 V.

4 General requirements for test switches

4.1 Material and workmanship

The test switch and its components shall be substantially constructed of suitable material in a workmanlike manner.

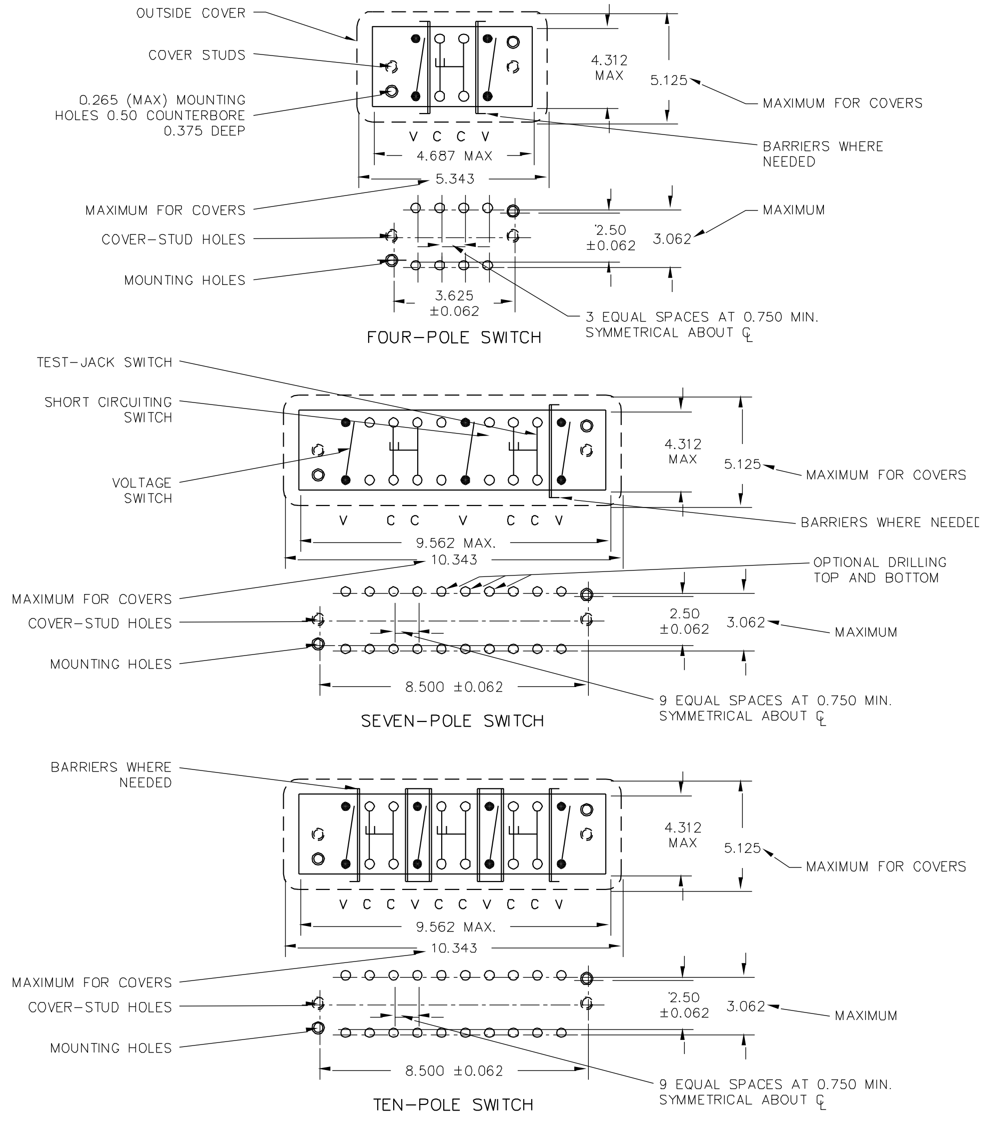
4.2 Nameplates

Nameplates are not required on these test switches, but a manufacturer's identifying marking (such as catalog number, trademark, etc.) shall be stamped, printed, affixed, or cast in a convenient place on each test switch. When required, a warning label indicating hidden internal jumpers should be affixed.

4.3 Movable parts

Movable conducting parts such as blade hinges shall be held in place by locknuts or pins or their equivalent, arranged so that a firm and secure connection will be maintained at any position of the switch blade.

ANSI C12.9 Test Switches



NOTES: (1) All dimensions are in inches.
(2) Unless otherwise specified, all tolerance shall be ± 0.015 inch.

ANSI C12.9 General Test Switch Specifications

1.1 Insulating barriers

When a voltage switch is installed adjacent to current switch or to another voltage switch at a different potential then for safety considerations the two switches shall be separated by an insulating barrier as indicated in figures 1 through 3. Barriers may be an integral part of the base, a separate part fastened to the base, or an integral part of each individual switch section.

1.2 Wiring terminals and test clips

1.2.1 Wiring terminals

Test switches shall be provided with suitable wiring terminals for the connection of AWG No. 14 to AWG No. 8 secondary conductors.

1.2.2 Test clips

Facilities for attaching test clips shall be provided on the terminals or on the wire binding screws.

1.3 Mounting holes

Mounting holes (two minimum) shall be of the dimensions shown in figures 1 through 3.

1.4 Cover

1.4.1 General

An insulated cover shall be available for the test switches and if used shall be held in place by cover studs. The cover may be made of glass, plastic or other suitable non-conducting material, but shall not exceed the maximum dimensions shown in figures 1 through 3. When the cover is in place, all switches shall be in a closed position.

1.4.2 Cover holes

The diameter of the cover-stud holes shall be 0.281 in., located as shown in figures 1 through 3.

1.4.3 Cover studs

Removable cover studs with suitable provisions for sealing shall be available for use in each instrument-transformer-meter test switch in the positions indicated in figures 1 through 3. The diameter of these studs shall not exceed 0.25 in. Standard instrument-transformer-meter test switches shall be provided either with or without cover studs.

1.5 Acceptable spacings

The minimum acceptable spacings shall be as indicated in table 2.

Table 2 – Minimum acceptable spacings

Voltage between parts involved (V)	Minimum spacings from live parts to			
	Parts of opposite polarity*		Grounded metal**	
	Over surface (in.)	Through air (in.)	Over surface (in.)	Through air (in.)
0-300***	0.750*	0.375*	0.500	0.375
301-600	1.250*	0.750	1.000	0.500

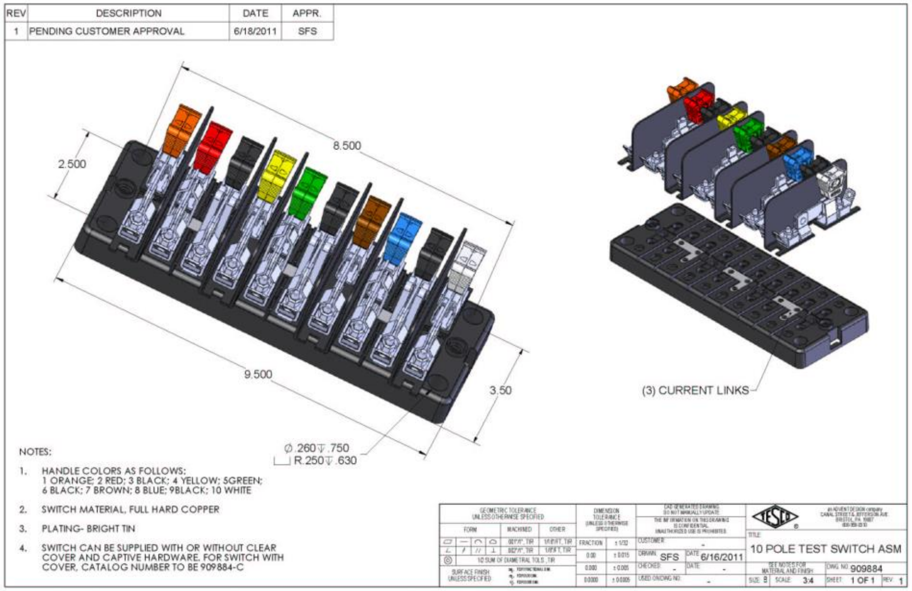
*To be acceptable at other than wiring terminals, through-air and over-surface spacings of 0.375 in between parts of opposite polarity shall withstand a special dielectric strength test at 6 000 V, 60 Hz, for 1 min.

**To be acceptable at other than wiring terminals, through-air and over-surface spacings of 0.375 in between current-carrying parts and cast-metal enclosure or grounded metal, where indentation or deformation of the overall enclosure will not affect spacings, shall withstand a special dielectric strength test at 6 000 V, 60 Hz, for 1 min.

***300 V spacings apply to a 600 V test switch, if the phase-to-neutral voltage does not exceed 300 V for spacings: (1) from neutral to phase-voltage parts, and (2) from neutral to grounded metal.

Test Switch Configurations

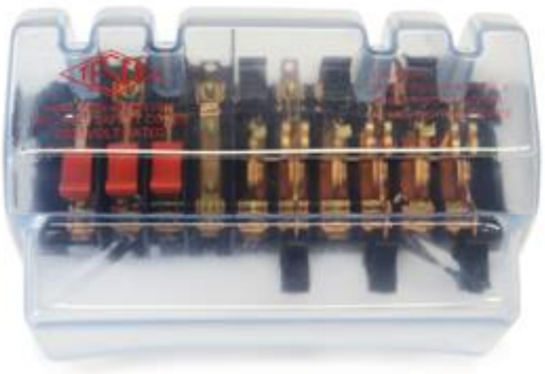
- Layout
- Handle Colors
- Reversed vs. Normal Potentials
- Current Links
- Base Sizing
- Barrier Locations and Removable vs Fixed



Test Switch Accessories

- Test Plugs
- Safety Covers
- Test Switch Isolators

On installations that contain Test Switches, test leads terminated with a test switch
safety test probe (test plug) should be used for CT testing. This provides a “make-before-break” connection to prevent accidental opening of the current transformer secondary loop.



ANSI C12.9 Test Jack Specifications

4.6 Provision for test plugs

Each double-pole short-circuiting current switch shall incorporate a test jack which is designed to permit the insertion of a test plug. The test-jack switch can be either in the left-hand or the right-hand position. In order to assure proper mating with the test plug the test jack shall conform to Figure 4.

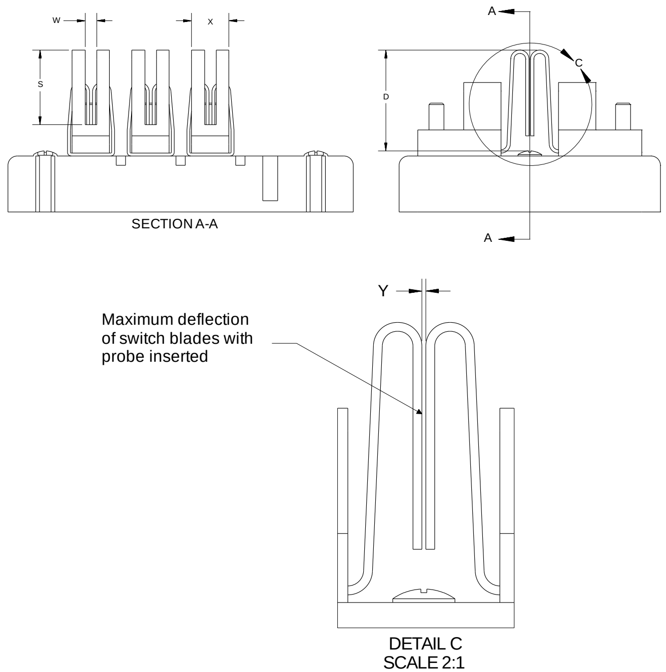


Figure 4 – Test switch typical cross section

Table 1 – Test switch dimensions

TEST SWITCH DIMENSIONS			
DIMENSION	**MINIMUM**	**PREFERRED**	**MAXIMUM**
S	**0.900**	**1.200**	**1.250**
W	**0.125**	**0.140**	**0.175**
X	**0.430**	**0.500**	**0.550**
D	**1.280**	**1.350**	**N/A**
Y			**0.188**

ANSI C12.9 Test Plug Specifications

1 General requirements for test plugs

1.1 Materials and workmanship

The test plug shall be constructed with an insulated handle providing an anti-slip gripping area and a barrier to help prevent the user's gloved hand from slipping into contact with the test switch.

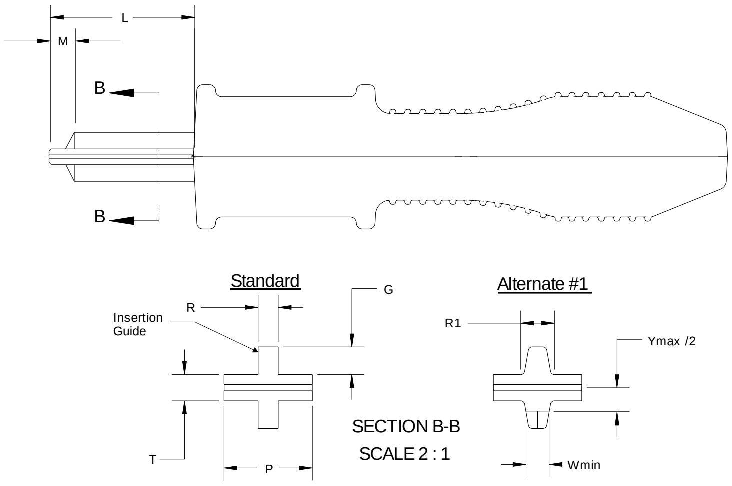


Figure 6 – Typical test plug

Notes:

(1) When the insertion guide takes the form of Section B-B Alternate #1, then for a switch with a slot width Wmin, the switch Jaws shall not be separated by more than Ymax = 0.188" when inserted.

(2) If a positive stop is provided on the probe blade to limit insertion depth of the probe to M by bottoming out against S of the switch, then L may exceed Lmax provided M < Dmin – Smax = 0.030".

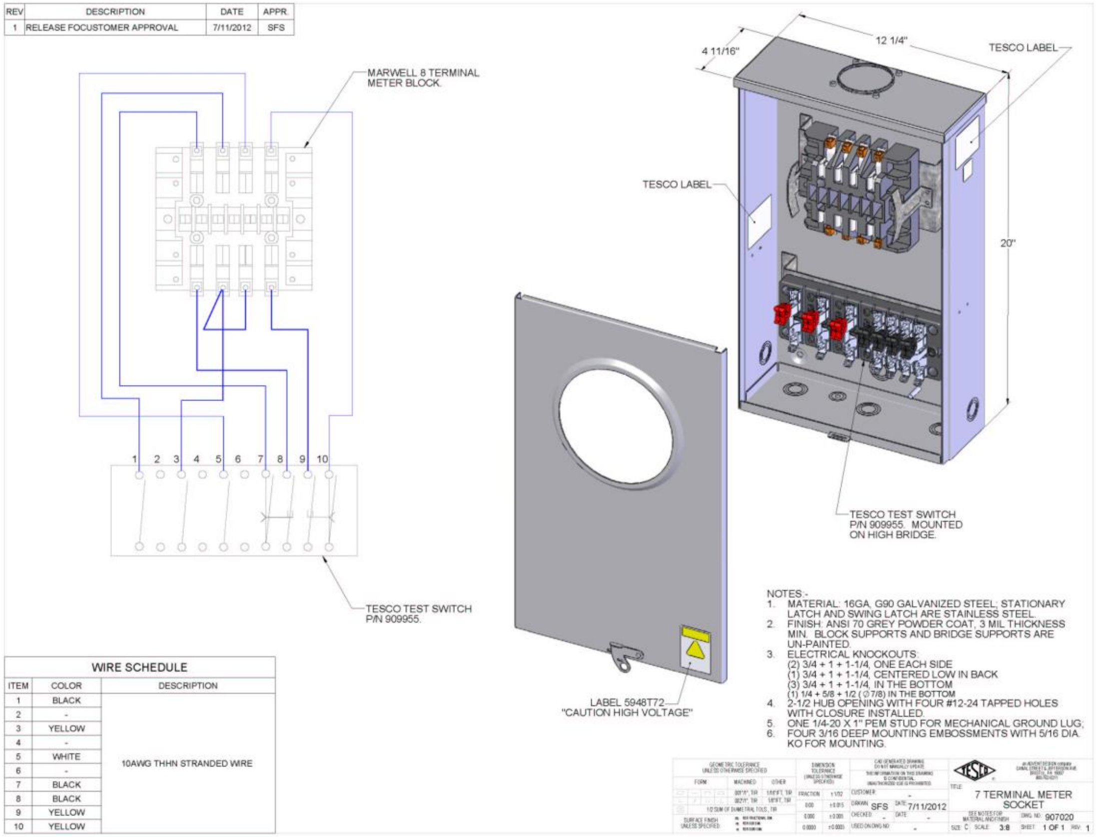
Table 3 – Test plug dimensions

TEST PLUG DIMENSIONS			
DIMENSION	**MINIMUM**	**PREFERRED**	**MAXIMUM**
L	**1.100**	**1.200**	**1.260**
M	**0**	**0.140**	**0.175**
R	**0.090**	**0.110**	**0.120**
R1	**n/a**	**n/a**	**0.156**
T	**0.100**	**0.130**	**0.156**
G	**0.040**	**0.125**	**0.175**

ALERT TO USERS: Prior to adoption of this standard there are known instances of probes and switches where interferences exist which may not allow all probes and switches to mate or which may lead to probes shorting to undesired conductors.

Pre-Wired Transformer Rated Enclosures

- Cover Types
- Wiring
- Sockets



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Hot Sockets- Issues, Causes and Best Practices

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THE ISSUE

- Hot Sockets are not a new phenomenon. Virtually every meter man has pulled a meter with a portion of the meter base around a blade melted and virtually every utility has been called to assist in the investigation of a fire at a meter box.
- AMI deployments because of the volume of meters involved put a spot light on this issue.
- What causes a hot socket?
- Are the meters ever the cause of a meter box failure?
- What are the things to look for when inspecting an existing meter installation?
- What are the best practices for handling potential hot sockets?
- This presentation will cover the results of our lab investigation into the sources for hot sockets, the development of a fixture to simulate hot sockets, the tests and data gleaned from hot sockets, and a discussion of "best practices" regarding hot sockets.

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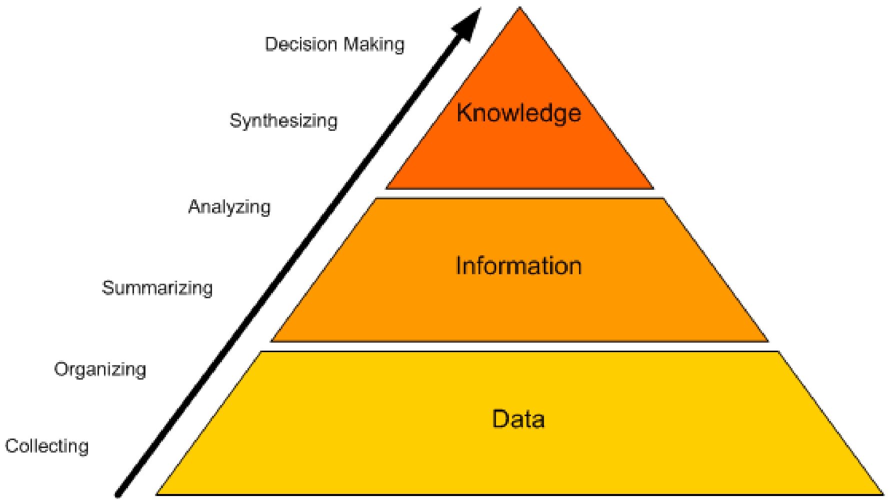
WHY DO WE KNOW ANYTHING ABOUT HOT SOCKETS?

- TESCO has been fortunate enough to be involved in several meter deployments where we supplied full time and part time meter engineers and project managers to our customer's AMI deployment teams. In this capacity we have been involved in evaluating hot socket issues and helping to determine an appropriate response to actual or potential hot sockets.
- TESCO's meter lab has been contracted to develop a laboratory fixture that would simulate the various features common to most hot sockets found in the field.
- TESCO developed and refined a fixture since 2013 running tests and gathering data on the effect of hot sockets on meters.
- TESCO has access to a large number of meters which have been exposed to hot sockets both before and after catastrophic failure.
- We have access to a limited number of sockets that were hot sockets and did not yet fail catastrophically.



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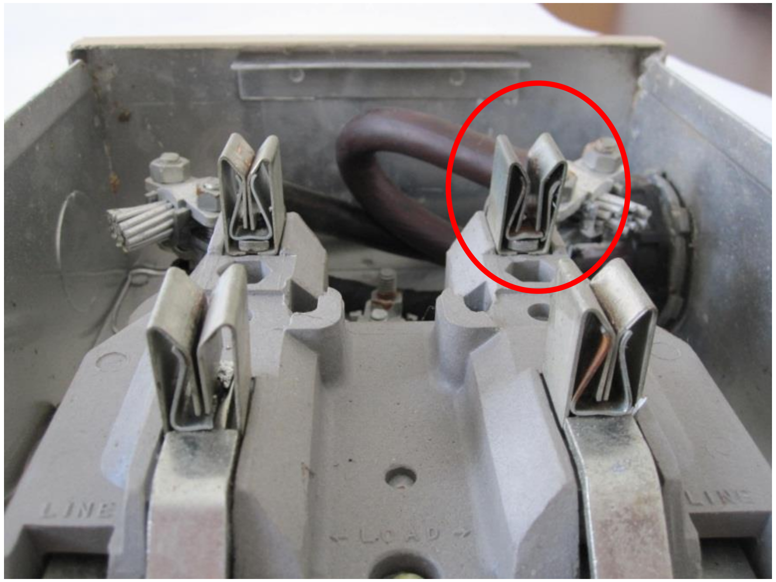
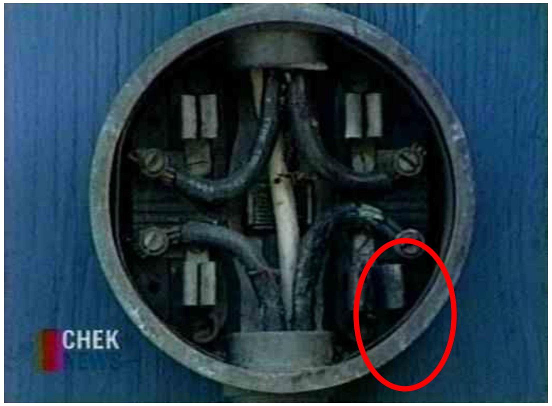
SEARCHING FOR HOT SOCKET SOURCES

Common Features and Common Sources of Concern



- Pitted and discolored meter blades
- Melted plastic around one or more of the meter stabs (typically the plastic around one stab is where the deformation starts)
- Pitted and discolored socket jaws
- Loss of spring tension in the socket jaws



Hot Socket Simulation Fixture

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EXPECTED & UNEXPECTED RESULTS

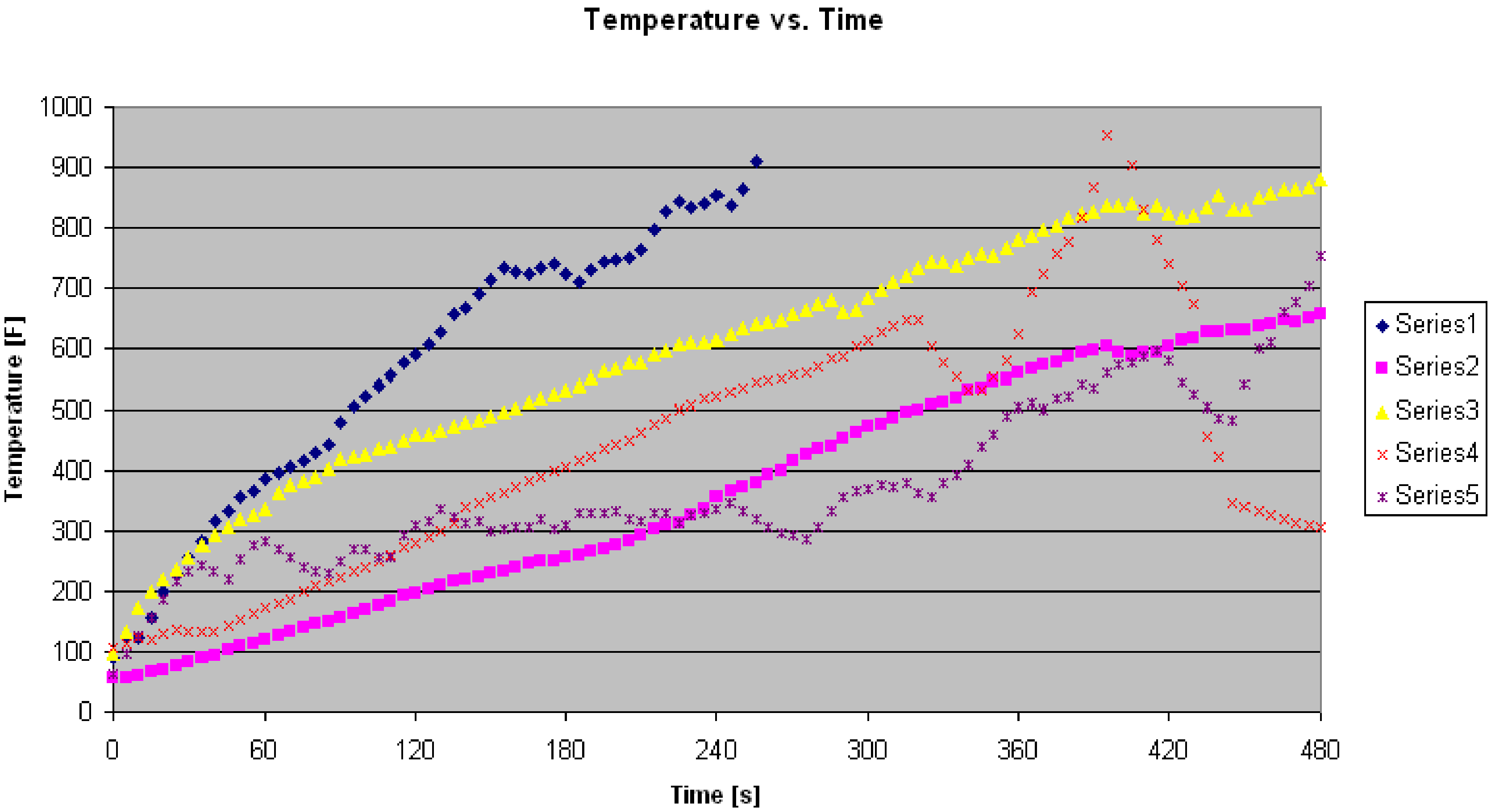
Expected:

- Hot Sockets are exactly that – hot sockets. The hot sockets are the source of the problem and not hot meters.
- Electromechanical meters withstand hot sockets better than solid state meters

Unexpected:

- Current plays only a small role in how quickly a meter will burn up. Meters were burned up nearly as quickly at 3 amps, 30 amps, and 130 amps.
- Relatively small amounts of vibration can be the catalyst in the beginning and eventual catastrophic failure of a hot socket. Note: Other catalysts include but are not limited to power surges, debris, humidity, salt water.
- Contact resistance plays no role in creating a hot socket

TEMPERATURE RISE DATA



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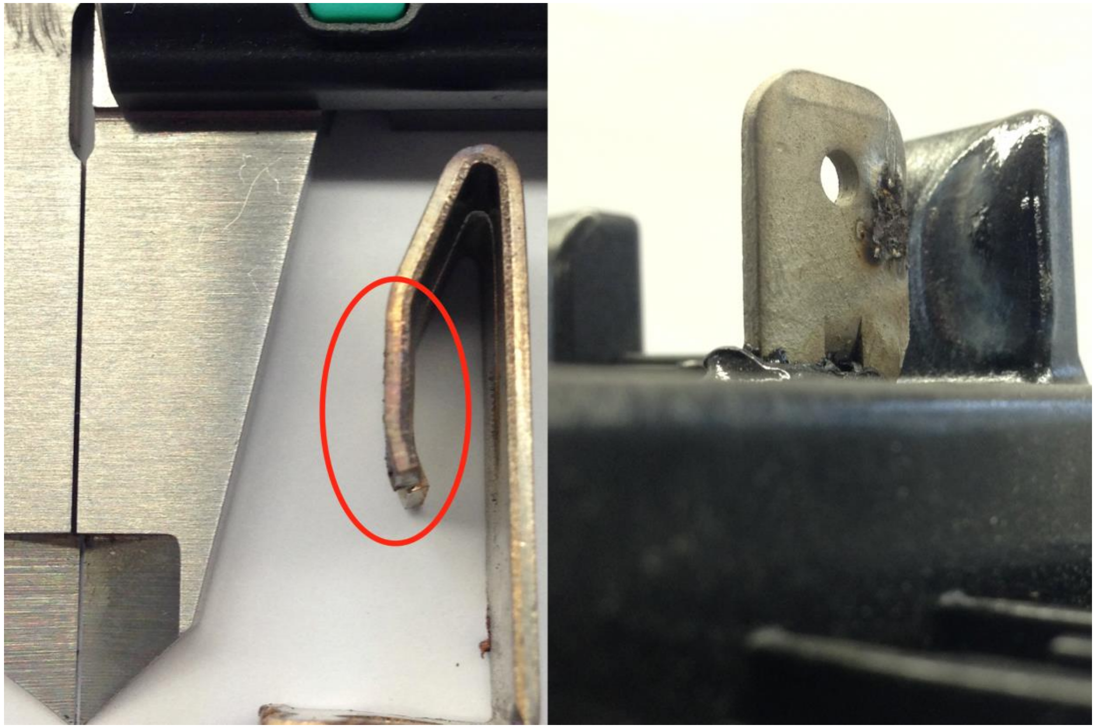
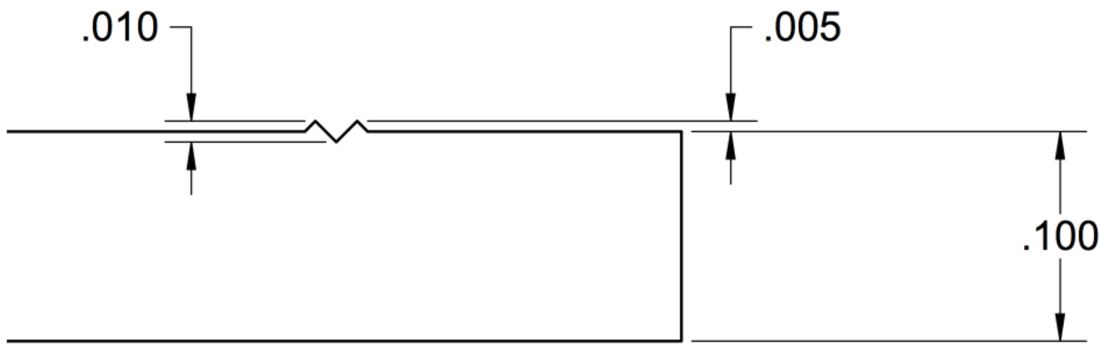
GAP EVALUATION

- Calipers show a .01” gap, with that size gap between jaws and stabs we were able to heat meter stabs over 1000 degrees Fahrenheit in a few minutes.
- The rough spots you see on the post-test jaw next to the calipers are over .005” high. This surface degradation appears on the stab as well.
- Between the two surfaces you can have large gaps, along with insulating by-product of the arcing, that can sustain heavy arcing in a solid state.



Service Degradation

- In a representative side view of a .1" thick standard meter stab, you can see how small these distortions appear relative to the thickness of the stab, while creating an air gap large enough for significant arcing.



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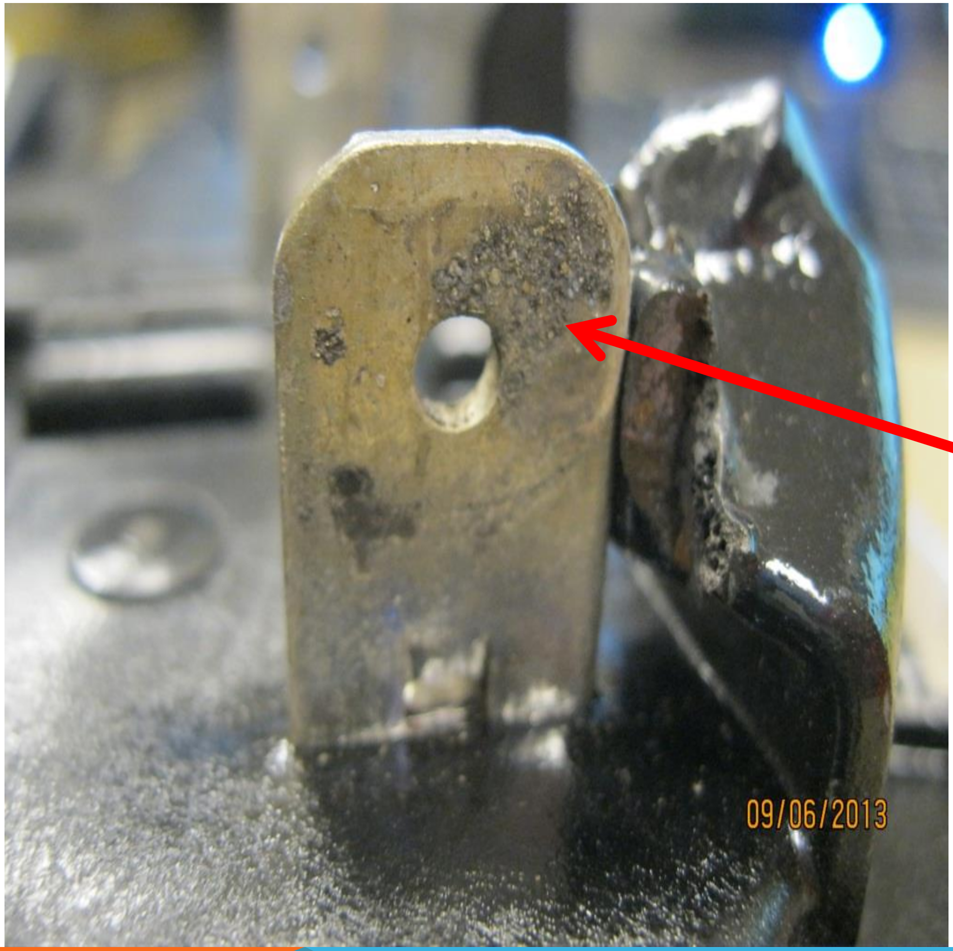
Jaw to Blade Arcing

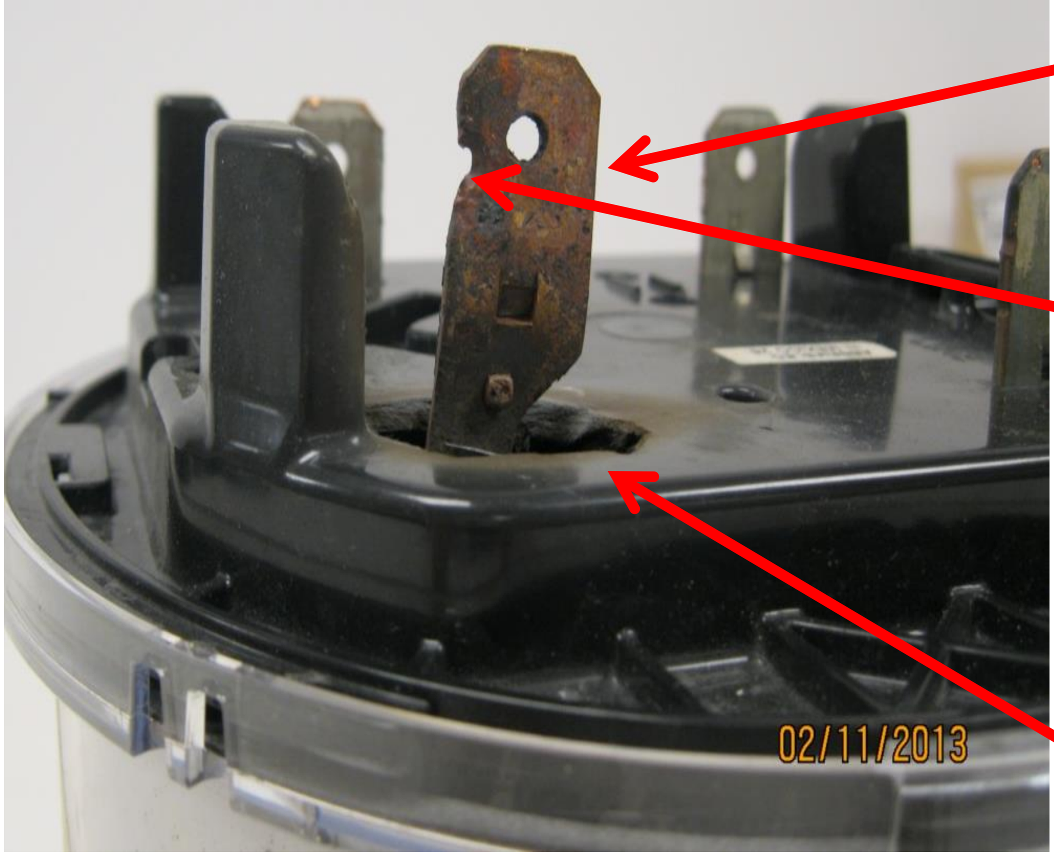


Jaws with intermittent connections will arc to the meter blade resulting in pitting on the blade.

Blade shows early signs of arcing.

Tin Melts at 232ºC which is lower than the 350ºC base plate plastic.

Severe Arcing Jaw to Blade



Tin burned off

Blade hole due to arcing to jaw – Copper melts at 1040ºC (1900ºF)

AX-SD base thermoset plastic melts at 960ºC (1760ºF)

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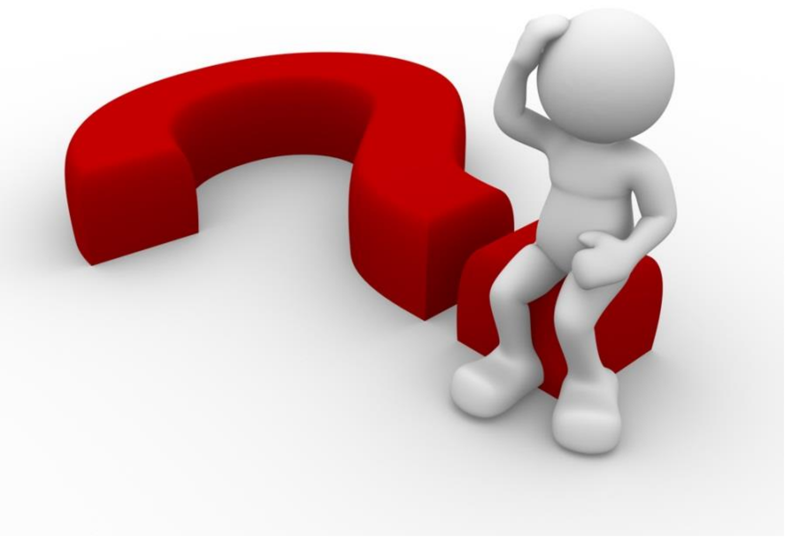
WHAT ARE THE NECESSARY INGREDIENTS FOR A HOT SOCKET?

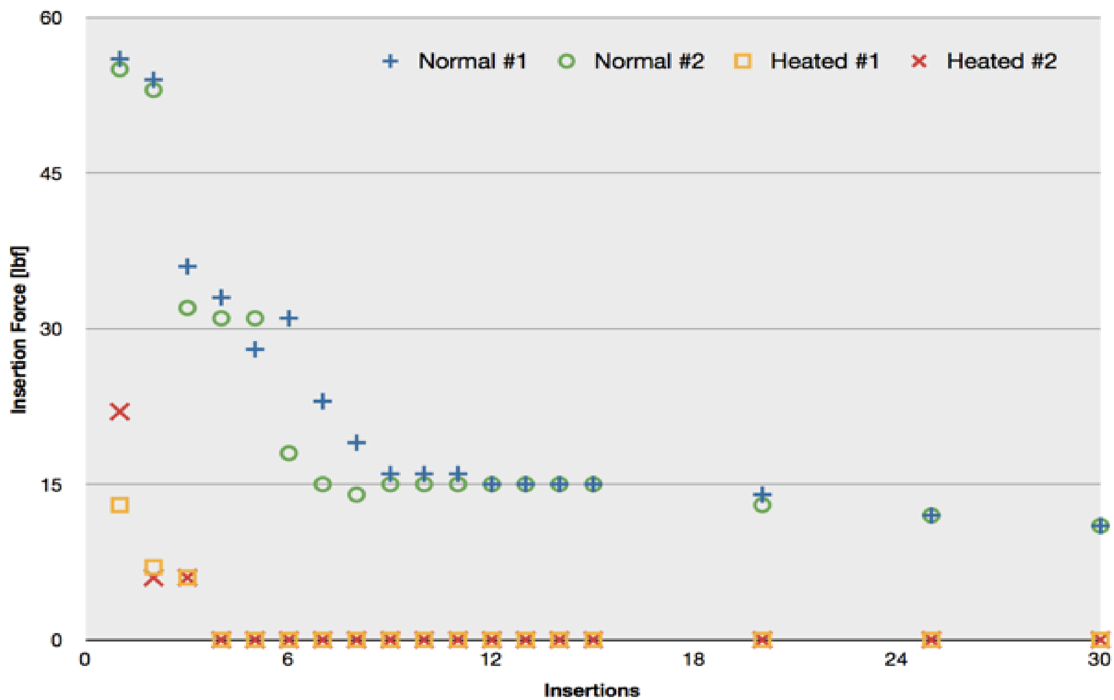
There are three necessary ingredients to create a hot socket (Note: We are not suggesting that we have simulated or even understand all causes for all hot sockets and meter related fires, but rather that we have simulated and understand the causes behind most hot sockets and meter related fires);

- Loss of jaw tension in at least one of the socket jaws.
- Vibration (or other catalyst to initiate arcing)
- Minimal load present



Insertions	Normal #1	Normal #2	Heated #1	Heated #2
1	56	55	13	22
2	54	53	7	6
3	36	32	6	6
4	33	31	0	0
5	28	31	0	0
6	31	18	0	0
7	23	15	0	0
8	19	14	0	0
9	16	15	0	0
10	16	15	0	0
11	16	15	0	0
12	15	15	0	0
13	15	15	0	0
14	15	15	0	0
15	15	15	0	0
20	14	13	0	0
25	12	12	0	0
30	11	11	0	0

Insertions, Heated Jaws vs Normal, Heated at 700°F for 5 minutes



FIELD INSPECTION OF SOCKETS
BEST PRACTICES

Example field check list

- Gaps in meter socket jaws
- Discoloration of one jaw vs. the other three
- Signs of melted or deformed plastic on meter base
- Pitting of either meter blade or socket jaw
- Loss of tension in meter socket jaws
- Check condition of wire insulation and connections to meter jaws
- Check the overall condition of the box, socket, meter and how they attach to each other and the building.
- Look for signs of tampering
- Look for signs of water or debris inside of the meter can

WHAT CAN BE DONE ONCE A HOT SOCKET IS IDENTIFIED?

- Easiest resolution is to replace the damaged jaw.
- Never try and repair a damaged jaw. The tension in the damaged jaw will not return simply by taking a pair of pliers and closing the jaw tighter.
- Either the entire box should be replaced or the damaged jaw (assuming the wiring and other jaws are deemed safe through the rest of the inspection.)

BASE LINE DATA ELECTRO MECHANICAL METERS VS SOLID STATE VS THE LATEST GENERATION OF METERS DESIGNED WITH HOT SOCKETS IN MIND

- At the start of our laboratory investigation the oldest electro mechanical meters withstood hot sockets the best
- The latest vintage solid state meters withstood hot sockets the least.
- Over the course of the past few years some meter manufacturers have begun to release meters designed to withstand hot sockets and some have even begun to put temperature sensing closer to the meter blades instead of only on the metrology boards.
- One meter vendor’s service switch meter has used high temperature base plate plastic since it was launched in 2008.)


SUMMARY

- Hot sockets start with a loss of tension in at least one of the meter socket jaws. This loss of tension can be from a variety of sources that start as early as improper installation or even “tight sockets”.
- Loss of tension is necessary to create the initial micro-arcing conditions.
- Sockets with repeated meter exchanges observed to have higher incidence of hot socket issues and “booting” a meter may spring jaws even more.
- Vibration appears to be the most common catalyst to the micro-arcing that creates the initial heat in a “hot socket”.
- The meter must have some power, but current is not a significant factor in how quickly or dramatically a hot socket occurs
- The effects of vibration and weakened jaw are cumulative
- Meter Manufacturers have all been working on the design of their meters to better withstand a hot socket. These new meters have better baseline performance than even the older electro mechanical meters, but a hot socket will eventually burn up even the most robust meter.

Questions?